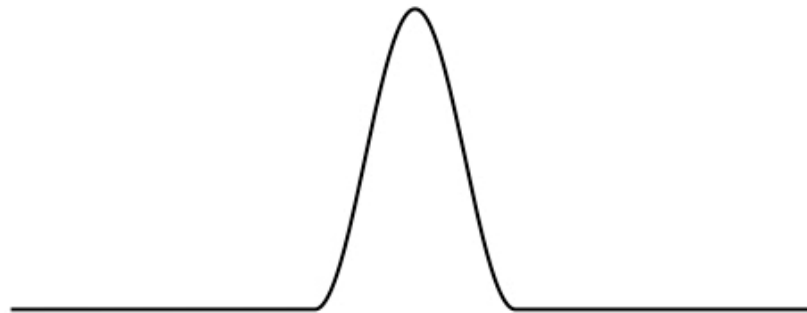
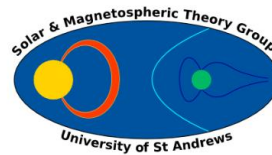


Phase Mixing of Partially Confined Alfvén Waves

Alex Prokopyshn, Alan Hood, Ineke De Moortel

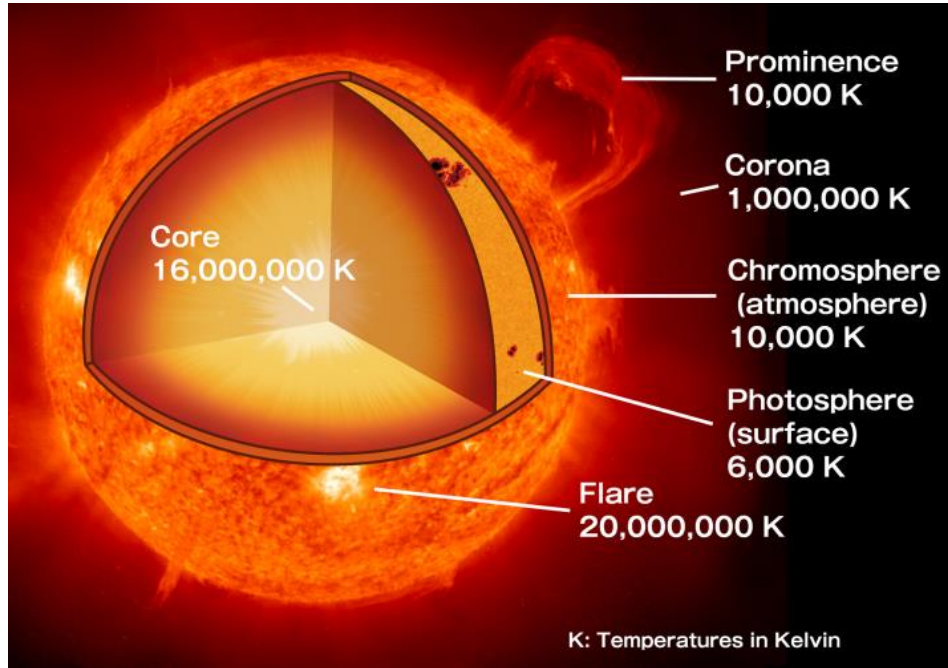


Aims

- Study continuous, footpoint driven Alfvén waves in coronal-like plasma.
- Analyse wave leakage through the transition region.
- Show that an upper limit for the gradients is reached.
- Calculate and present this upper limit.

Background

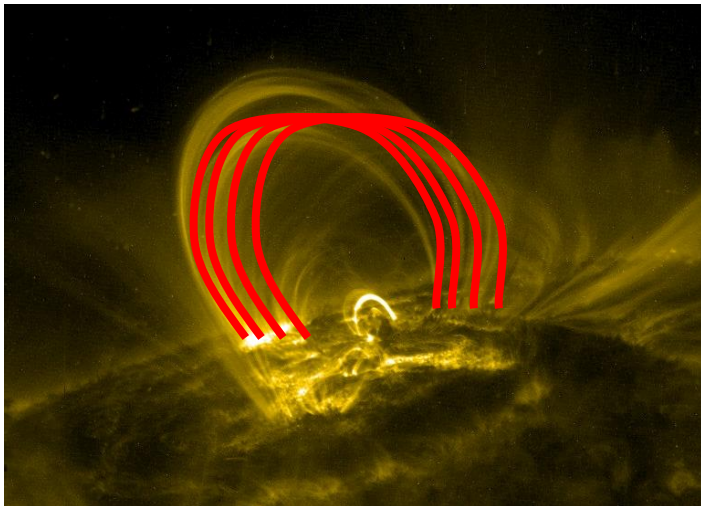
- Many proposed mechanisms for coronal heating, e.g. turbulence, phase mixing, nanoflares etc..
- It is difficult to show which mechanisms are dominant (if any).



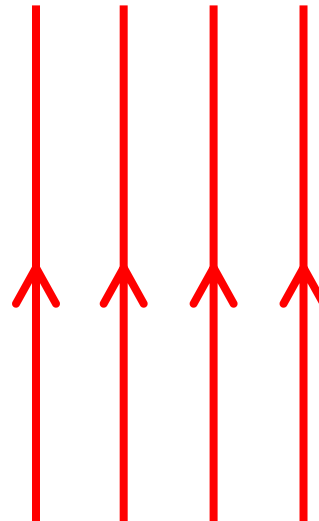
Source: aasnova.org

Background

- Can we quantify an upper bound for the heating provided by phase mixing?
- Estimate a parameter space where phase mixing is negligible.
- Upper bound is easier to find than an accurate value.



≈



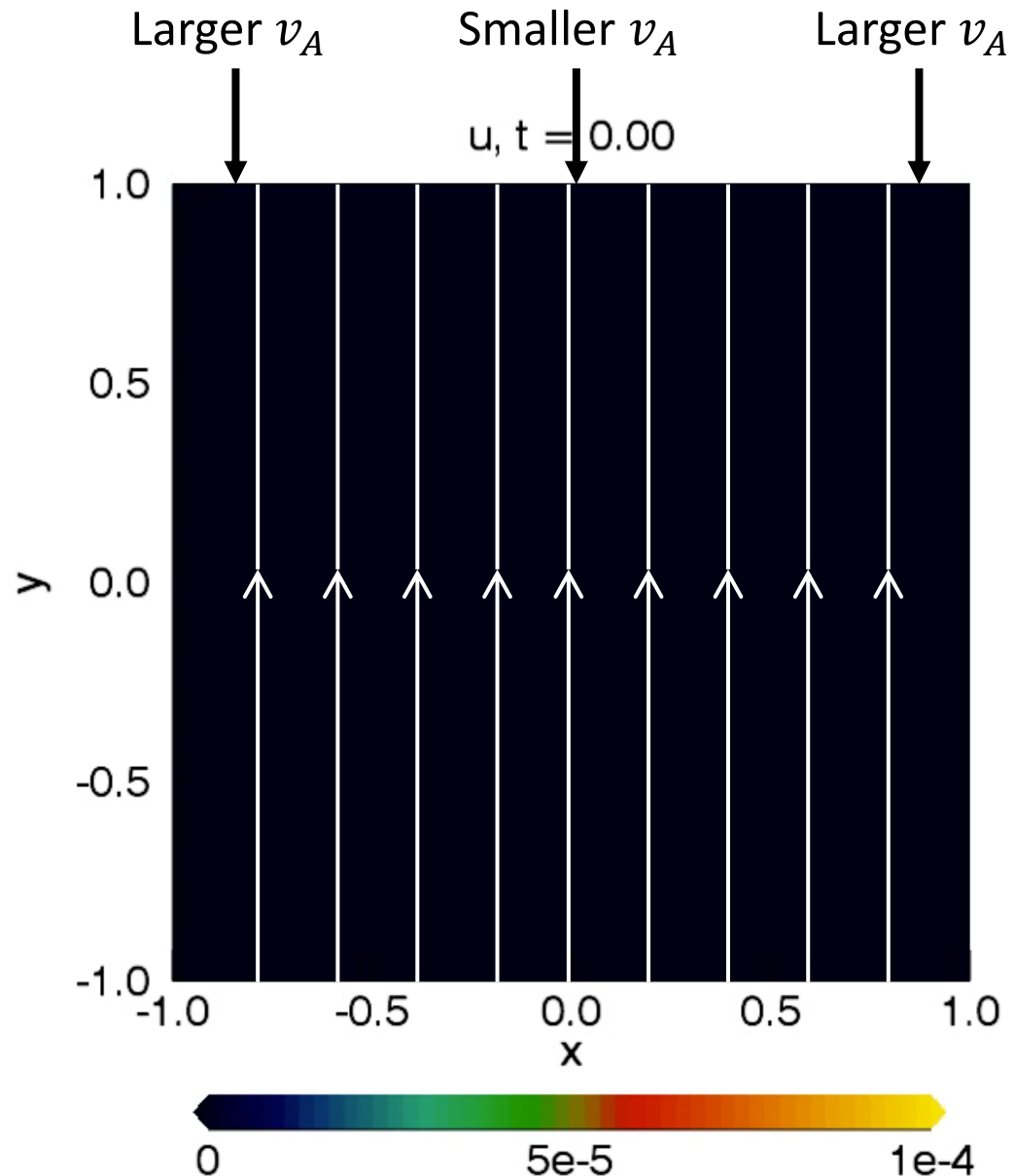
Source: TRACE, 171 Å,
Characteristic temperature $\approx 6 \times 10^5 \text{K}$

Phase mixing

$$\underbrace{\nabla_{\perp} v_A \Rightarrow \uparrow \nabla_{\perp} u, \nabla_{\perp} b}_{\text{This process = phase mixing.}}$$

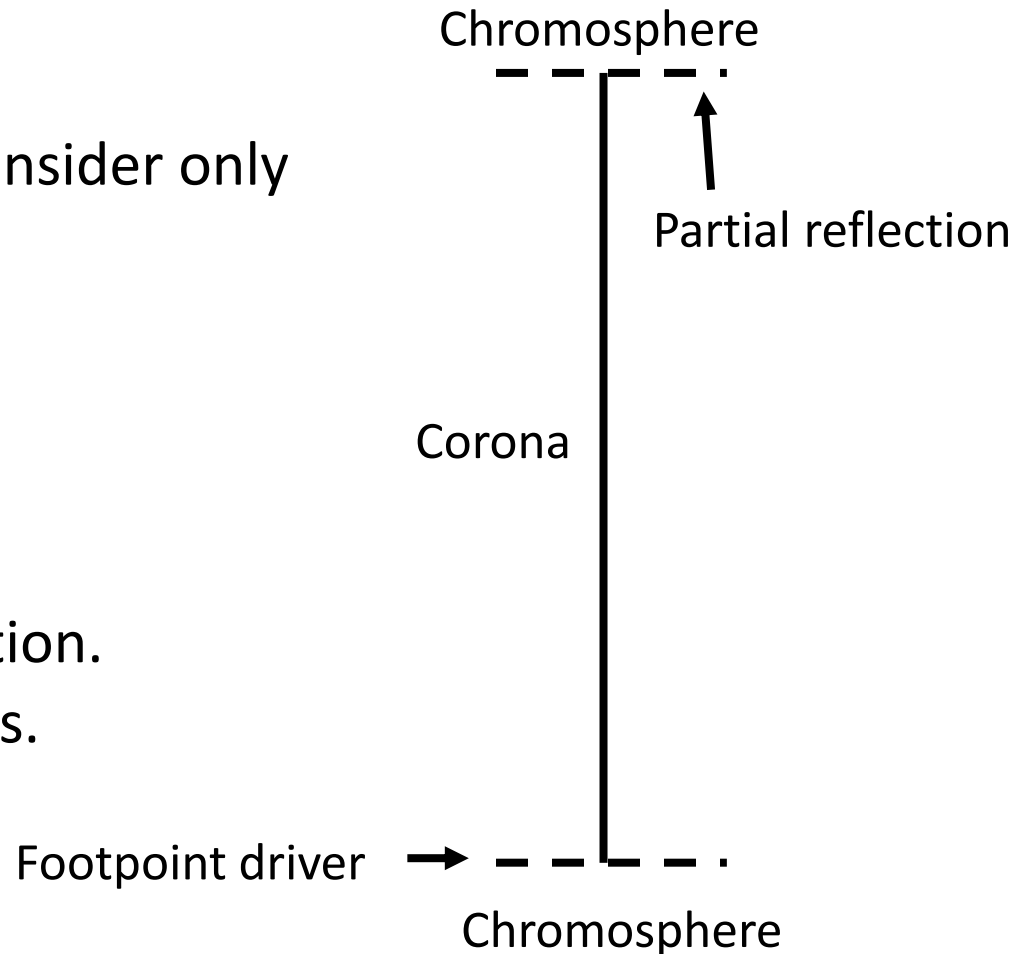
This process = phase mixing.

- In ideal MHD phase mixing is only responsible for changes to ∇_{\perp} not ∇_{\parallel} .
- Ohmic heating rate of an Alfvén wave is given by $|\nabla b|^2 / \sigma$.



Our model of a coronal loop

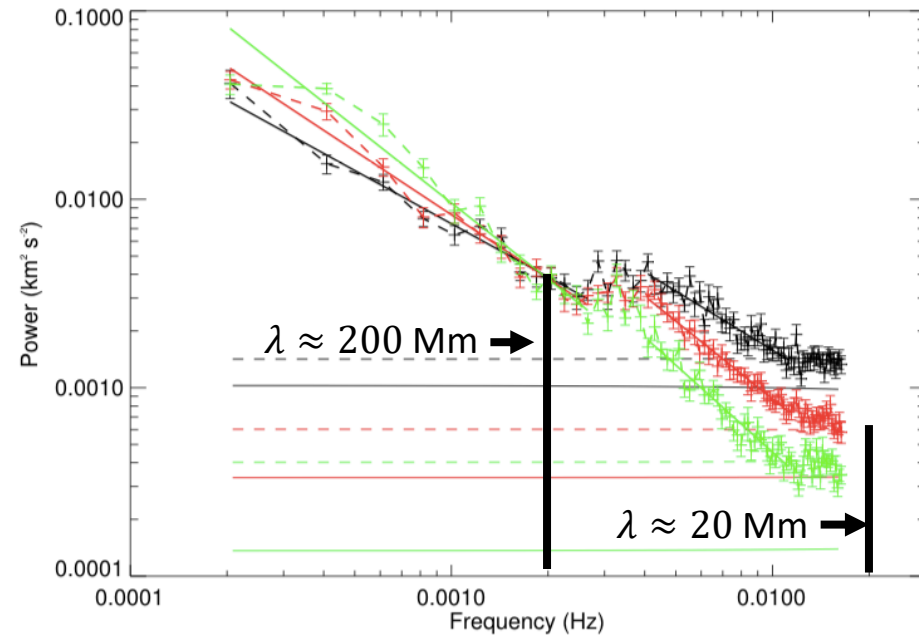
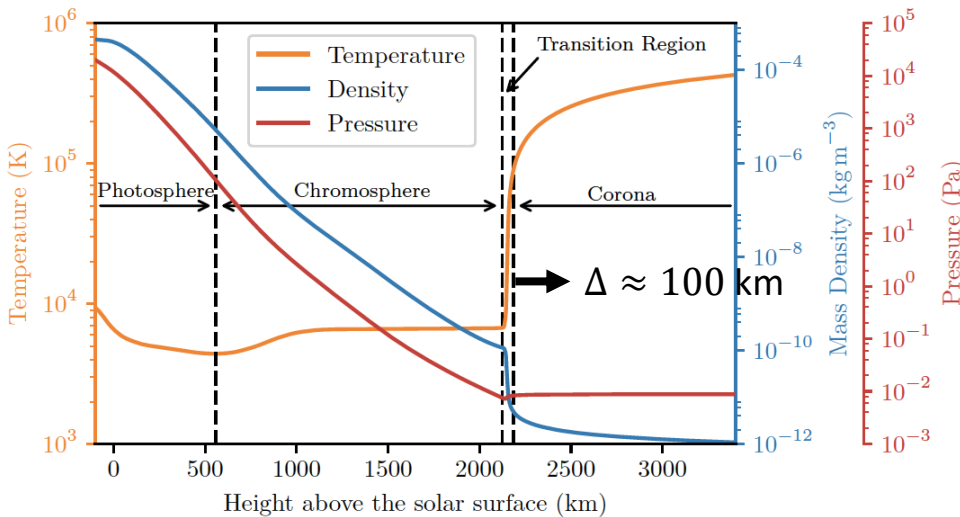
- Model loop in 2.5D, but consider only one field line.
- $\nabla_{||} v_A = 0^*$.
- $\nabla_{\perp} v_A \neq 0$.
- Ideal MHD.
- Linear waves.
- There is an invariant direction.
- Consider only Alfvén waves.



Structure

- Estimate wave reflection/transmission coefficient.
- Experiment 1:
 - Full reflection, sinusoidal driver.
- Experiment 2:
 - Partial reflection, sinusoidal driver.
- Experiment 3:
 - Partial reflection, broadband driver.
- Conclusions

The transition region is approximately a discontinuity in comparison to the wavelength of observed waves

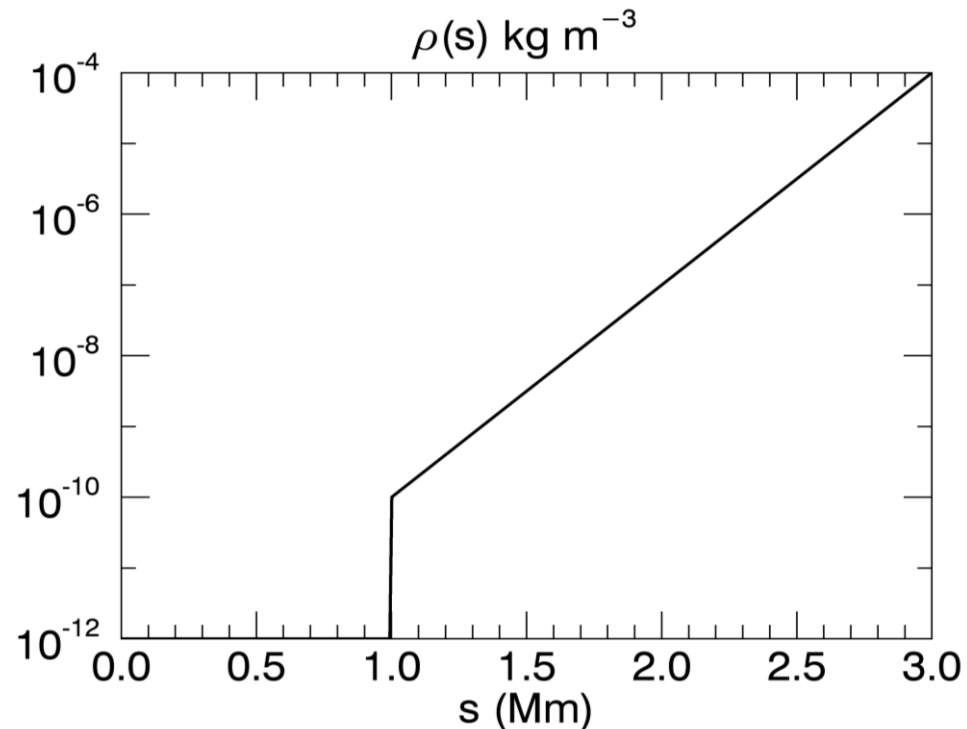


- Plasma values given by VAL model of the solar atmosphere.

- Power spectrum from Morton et al. (2016).
- Used COMP
- Cadence ≈ 0.03 Hz

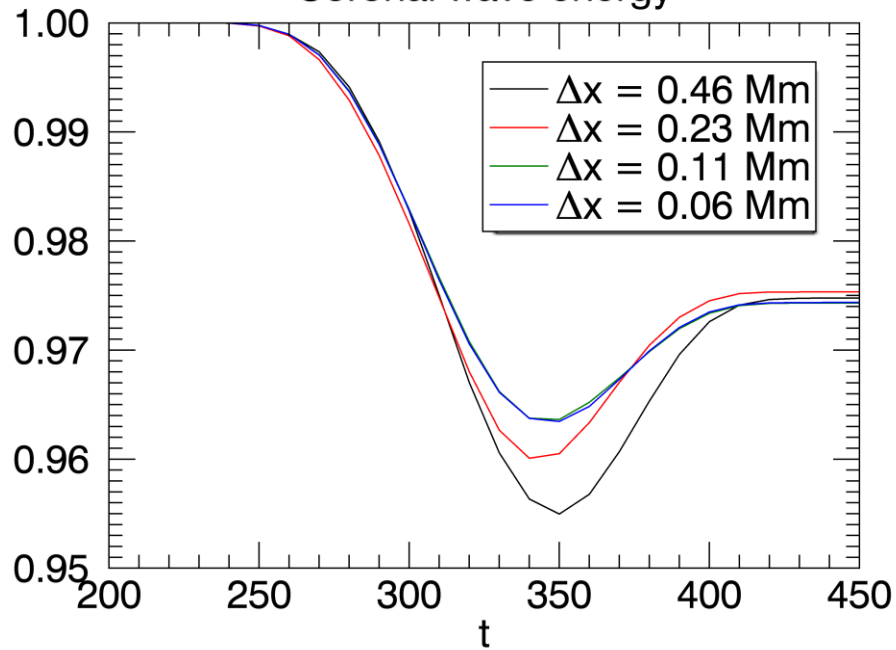
Estimating the energy reflection coefficient (R_E)

- Use LARE2D (but only 1 cell wide).
- Use density values based on VAL.
- Send in an Alfvén pulse and measure how much energy reflects and transmits.

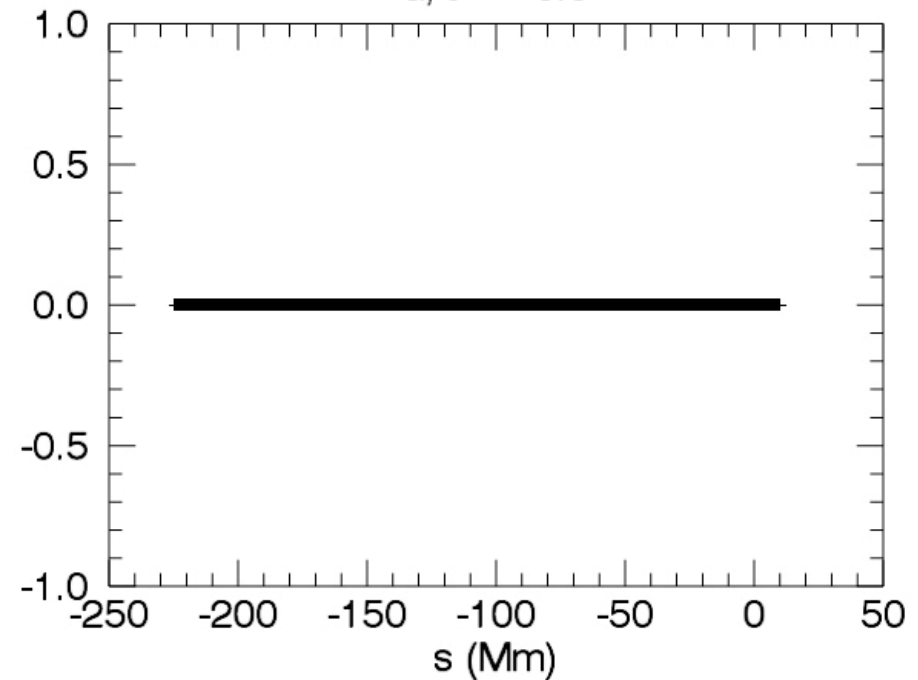


Calculating the energy reflection coefficient (R_E)

$\lambda = 200\text{Mm}$
Coronal wave energy



Velocity Amplitude
 $u, t = 0.0$



Energy reflection coefficient (R_E)

Grid size (Δs) (Mm)	R_E ($\lambda = 20$ Mm) ($P \approx 50$ s)	Grid size (Δs) (Mm)	R_E ($\lambda = 200$ Mm) ($P \approx 500$ s)
$\approx 5.9 \times 10^{-2}$	≈ 0.843	$\approx 4.6 \times 10^{-1}$	≈ 0.975
$\approx 2.9 \times 10^{-2}$	≈ 0.838	$\approx 2.3 \times 10^{-1}$	≈ 0.975
$\approx 1.5 \times 10^{-2}$	≈ 0.841	$\approx 1.1 \times 10^{-1}$	≈ 0.974
$\approx 0.7 \times 10^{-2}$	≈ 0.839	$\approx 0.6 \times 10^{-1}$	≈ 0.974

Analytic check of R_E

- R_E of the configuration on the right is

$$R_E = \left(\frac{\sqrt{\rho_2} - \sqrt{\rho_1}}{\sqrt{\rho_1} + \sqrt{\rho_2}} \right)^2.$$

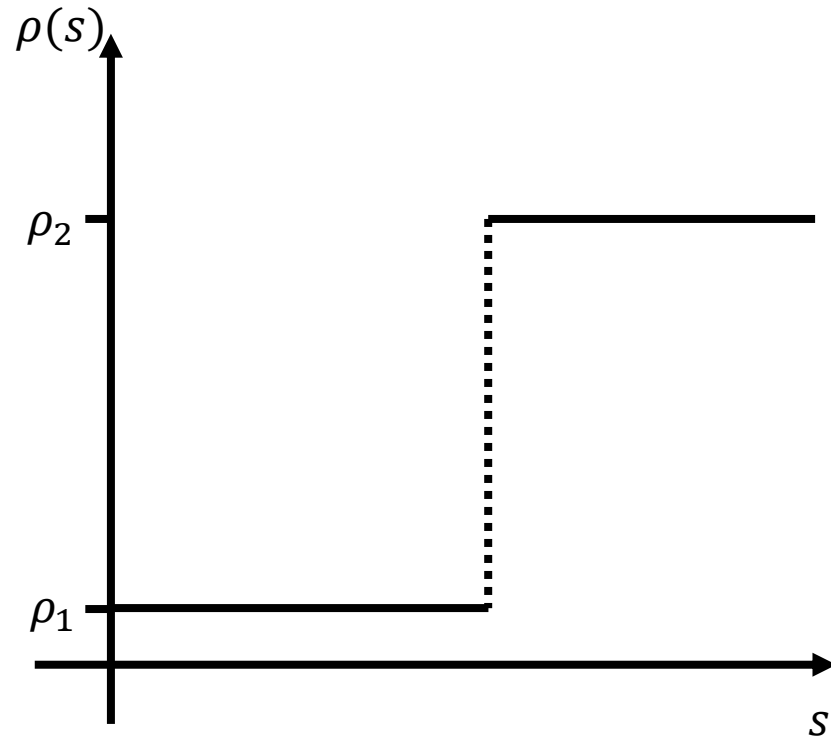
- For $\frac{\rho_2}{\rho_1} = 100$ this gives

$$R_E \approx 0.77.$$

- This is less than R_E for numerical experiments as expected.

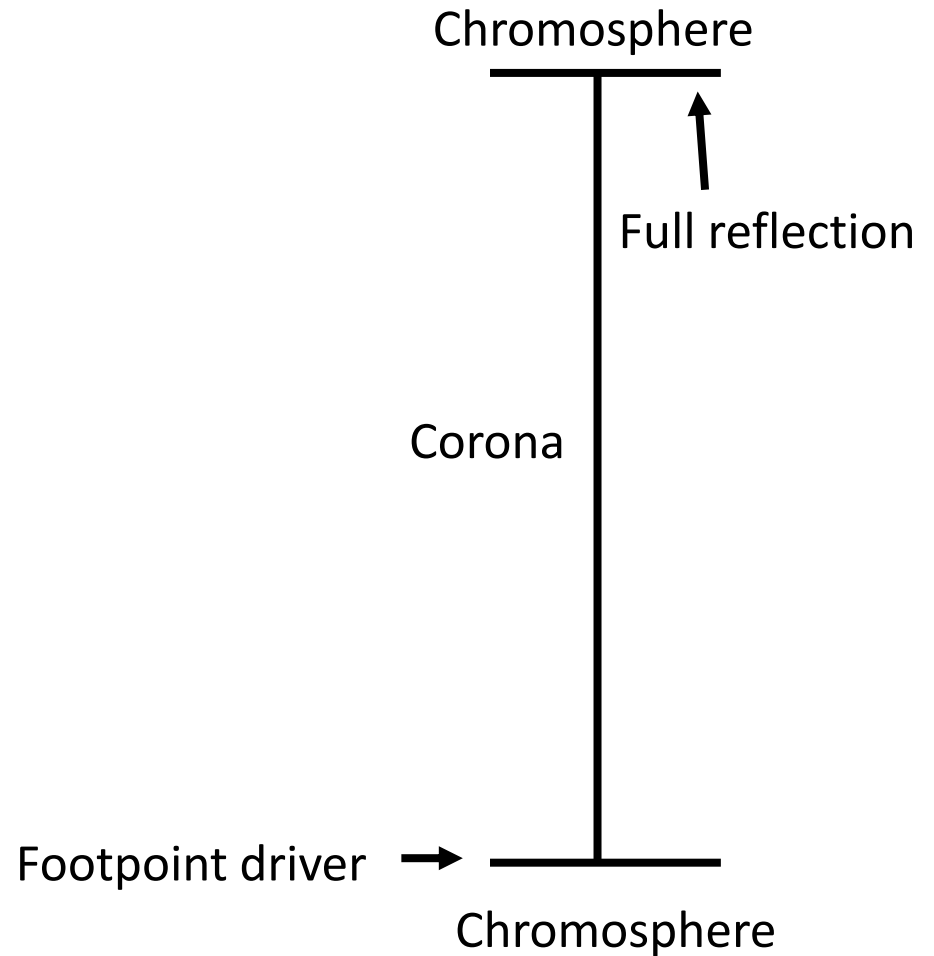
- For $\frac{\rho_2}{\rho_1} = 1000$ this gives

$$R_E \approx 0.88.$$



Experiment 1/3

- Full reflection ($R = 1$).
- Sinusoidal driver.



Analytic solution

- Solve the wave equation.

$$\frac{\partial^2 u}{\partial t^2} = v_A^2 \frac{\partial^2 u}{\partial s^2}$$

- Domain: $-l \leq s \leq l$

- Conditions:

- Driver: $u(-l, t) = \sin(\omega t)$

- Require a factor $R \leq 1$ to reflect at $s = \pm l$.

- Solve using d'Alembert's formula.

Analytic solution

Heaviside step function

$$u = \sum_{k=0}^m (-1)^k R^k H(\theta_k) \sin(\omega \theta_k),$$

$$\theta_k = t - (-1)^k \frac{s}{v_A} - \frac{2k+1}{v_A} l,$$

$$m = \left\lfloor \frac{tv_A}{L} \right\rfloor.$$

Floor function

Numerical solution

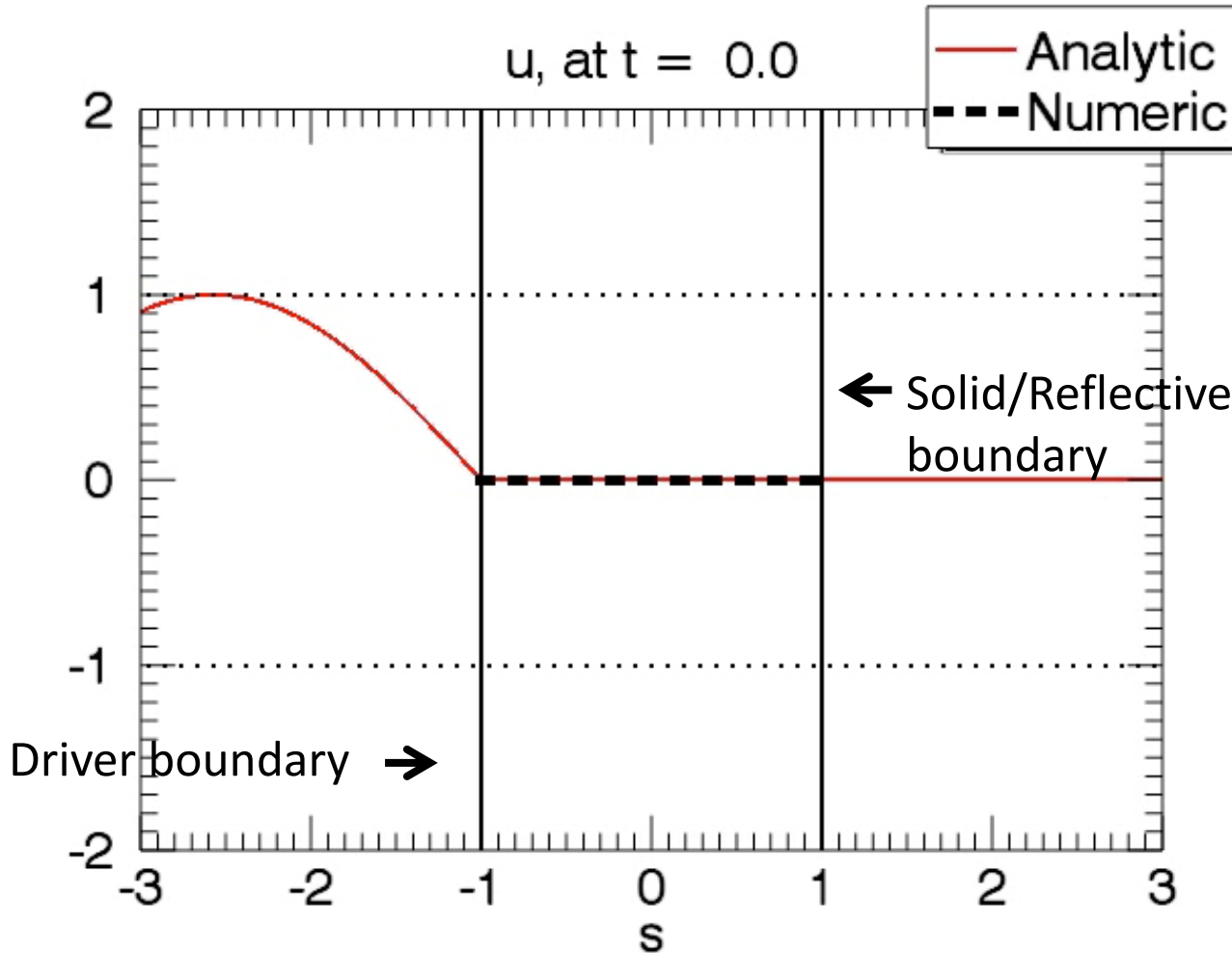
- Obtained using LARE2D.
- Linear driver imposed on the left boundary of the form:

$$u = 10^{-4} \sin(\omega t).$$

- Solid boundary conditions otherwise.

Numeric vs Analytic

Non-resonant driver



Solution for a resonant driver

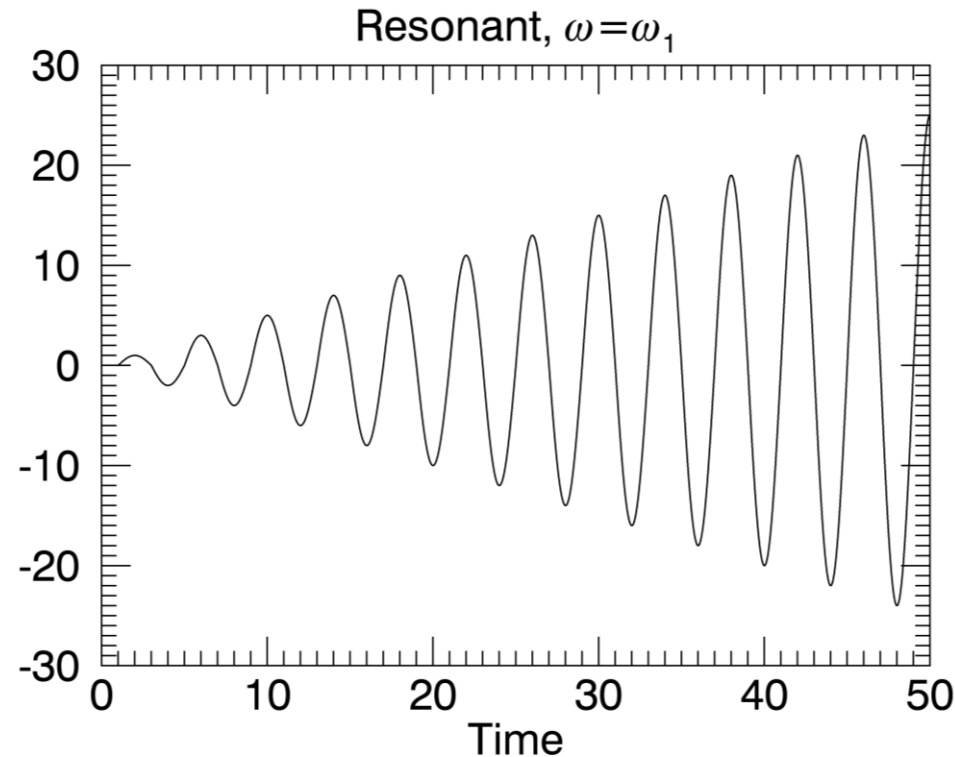
Amplitude, u , at loop apex

- The natural frequencies are given by,

$$\omega_n = n \frac{v_A}{L} \pi.$$

- If $\omega = \omega_n$, $n = \text{odd integer}$, then the solution is

$$u \approx \pm t \frac{v_A}{L} \cos(\omega t).$$



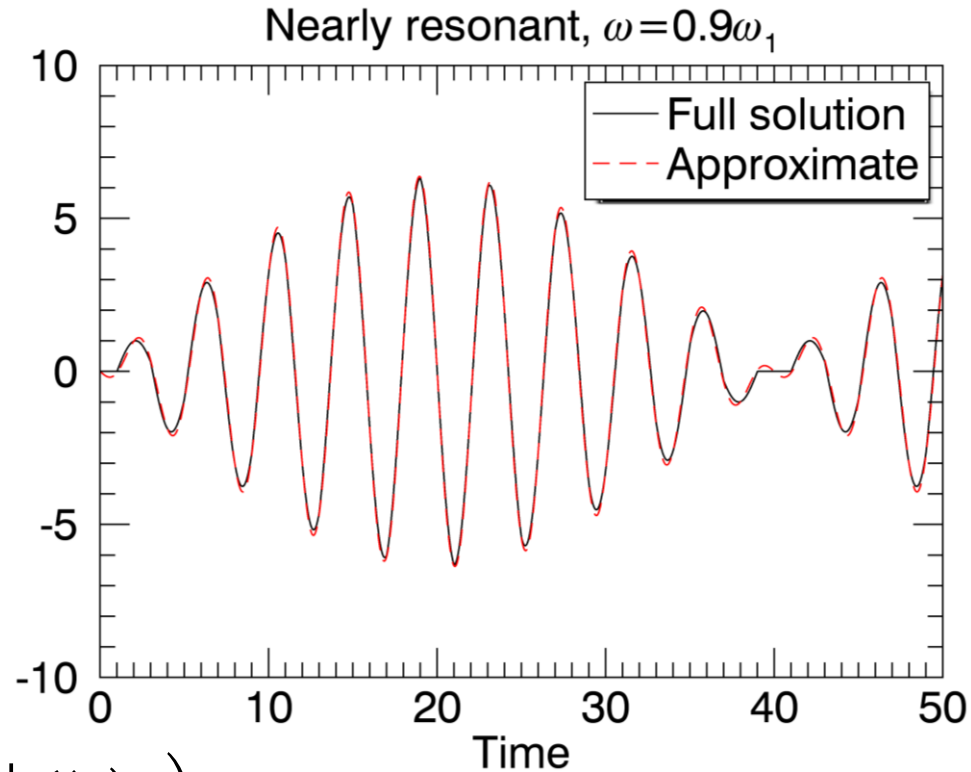
Solution near resonance

Amplitude, u , at loop apex

- If $\omega \approx \omega_n$, $n = \text{odd integer}$ then the solution is,

$$u \approx \sec\left(\frac{\omega l}{v_A}\right) \sin\left(\left(\frac{\omega - \omega_n}{2}\right)t\right) \cos\left(\left(\frac{\omega + \omega_n}{2}\right)t\right).$$

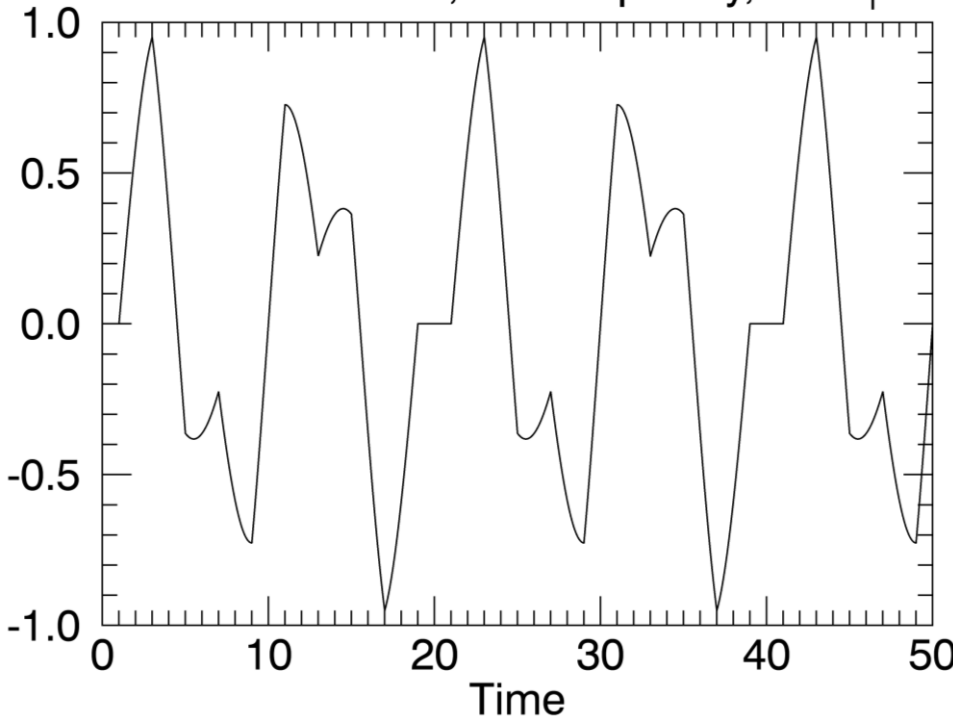
Beating frequency. ↑



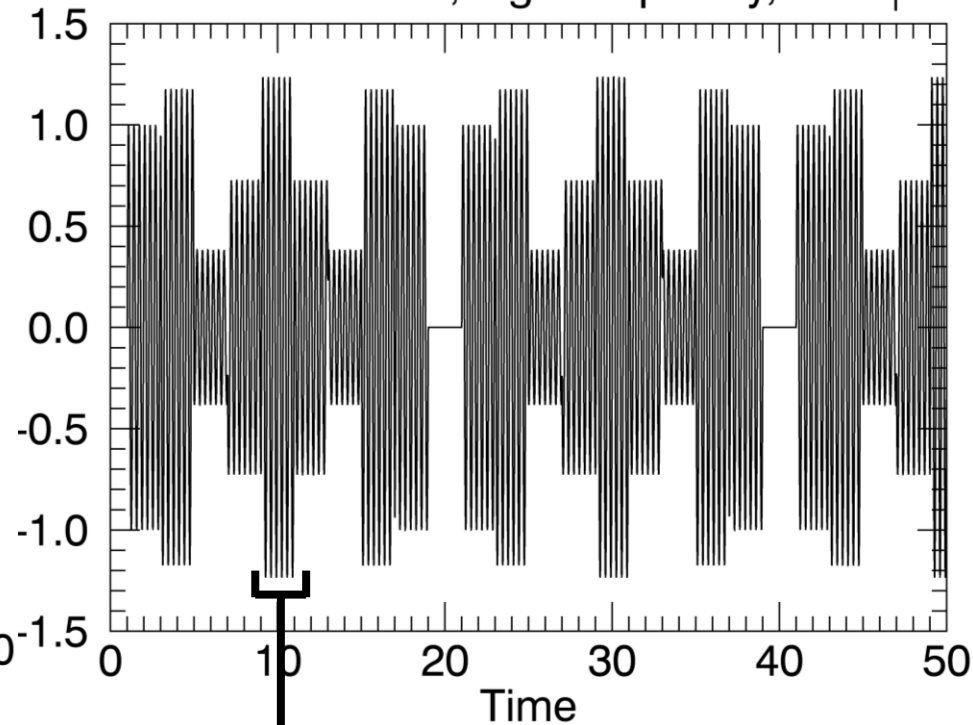
Solution away from resonance

Amplitude, u , at loop apex

Non-resonant, low frequency, $\omega < \omega_1$



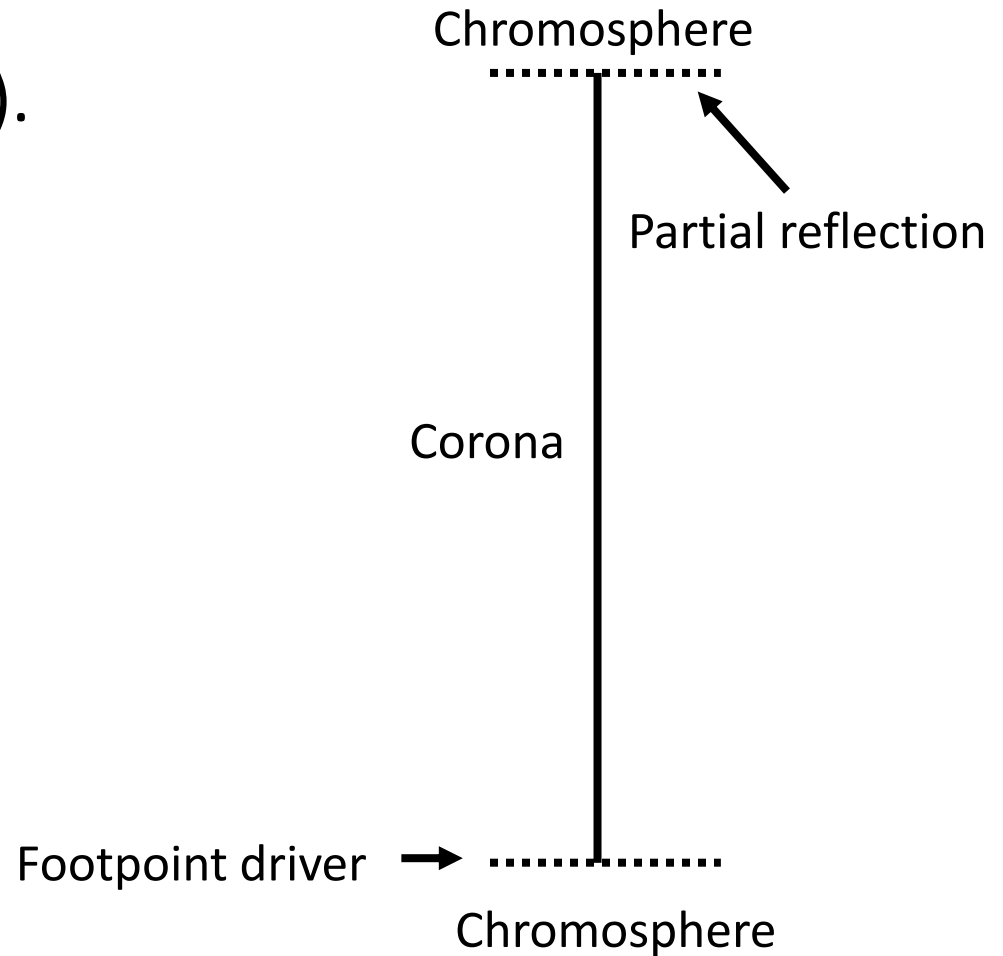
Non-resonant, high frequency, $\omega > \omega_1$



$$\Delta t = \frac{L}{v_A}$$

Experiment 2/3

- Parital reflection ($R < 1$).
- Sinusoidal driver.



Analytic solution

- Same as before, except now $R < 1$.

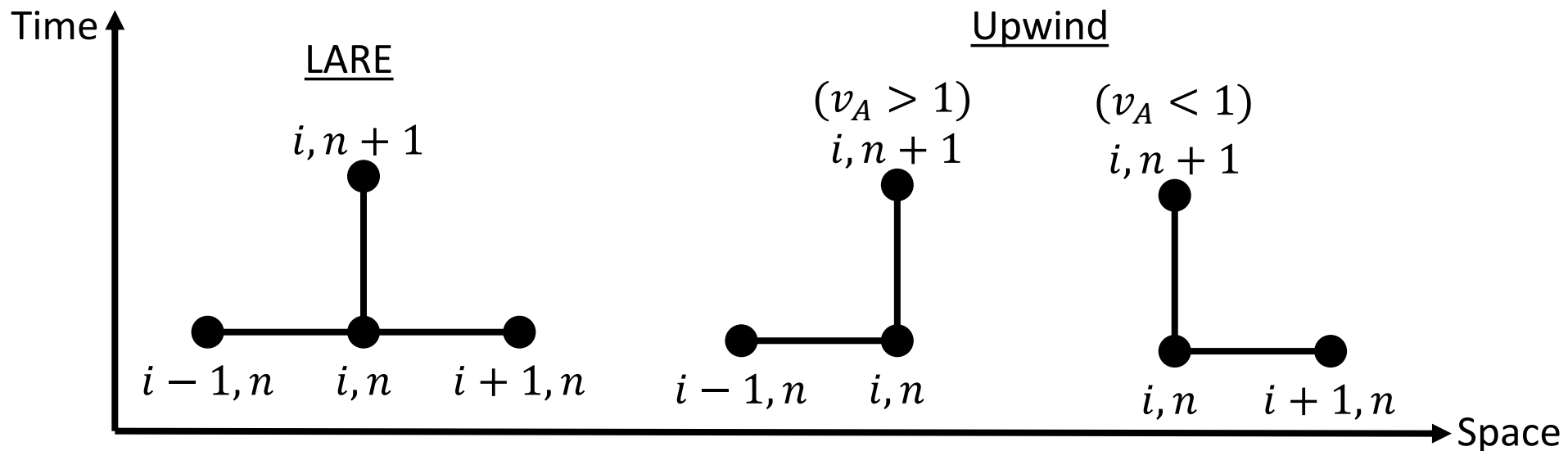
$$u = \sum_{k=0}^m (-1)^k R^k H(\theta_k) \sin(\omega \theta_k),$$

$$\theta_k = t - (-1)^k \frac{s}{v_A} - \frac{2k+1}{v_A} l,$$

$$m = \left\lfloor \frac{tv_A}{L} \right\rfloor.$$

Numerical solution

- Difficult to implement in LARE.
- We need an arbitrary amplitude to reflect.
- Decided it would be easier to make a linear upwind code.
- Stencil diagram:



Numerical solution

- Upwind code solves for the Elsässer variables,

$$z^{\pm} = u \pm b.$$

- Elsässer variables satisfy the advection equation,

$$\frac{\partial z^{\pm}}{\partial t} \mp v_A \frac{\partial z^{\pm}}{\partial s} = 0.$$

- Hence, z^+ travels in the negative direction and z^- travels in the positive direction.

Numerical solution

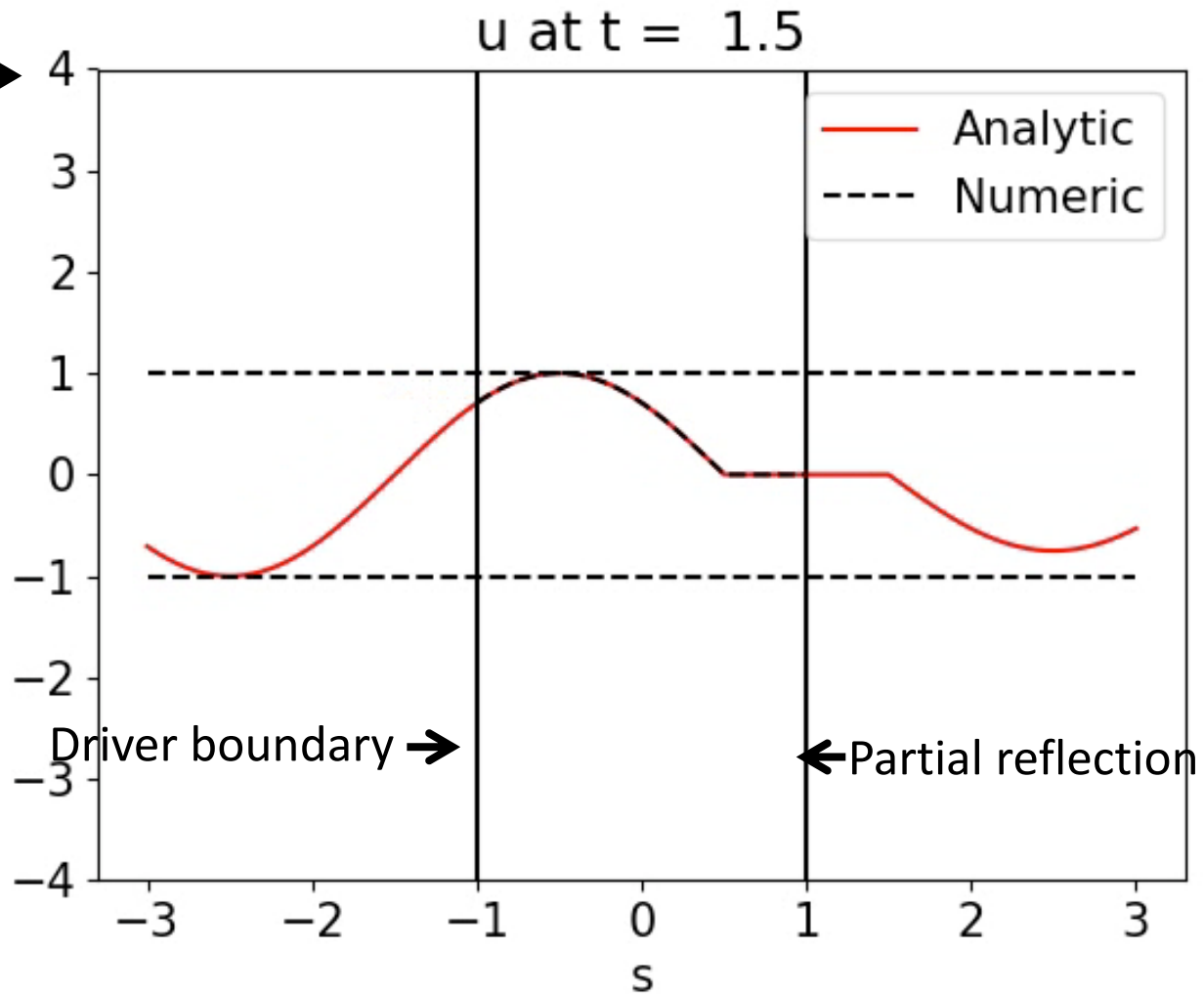
- To generate a driver, z^- is imposed on the left boundary.
- A factor $z^+ = Rz^-$ is generated at the right boundary and $z^- = Rz^+$ at the left boundary.
- This simulates partial reflection.

Numeric vs Analytic

Resonant driver

Steady-state amplitude →

- $R = 3/4$.
- Maximum amplitude reached despite being ideal and resonant.



Why does the system reach a steady-state?

- Intuitive reason:
 - A wave losing energy through leakage is in some sense equivalent to a wave losing energy via diffusion.
 - Hence, a steady-state is reached for the same reason it does if the wave is damped.
- Mathematical reason:
 - The solution can be rewritten as a geometric series, which converges to a finite value for $R < 1$.

Writing the solution as a geometric series

$$u = \sum_{k=0}^m (-1)^k R^k H(\theta_k) \sin(\omega \theta_k),$$

$$\theta_k = t - (-1)^k \frac{s}{v_A} - \frac{2k+1}{v_A} l,$$

$$m = \left\lfloor \frac{tv_A}{L} \right\rfloor,$$

let $s = 0$ and replace $\sin()$ with $\exp(i)$,

$$u = e^{i\omega t - l/v_A} \sum_{k=0}^{m-1} (-1)^k \left(R \cdot e^{-\frac{2i\omega l}{v_A}} \right)^k + (-1)^m R^m H(\theta_m) e^{i\omega \theta_m},$$

let $t \rightarrow \infty$,

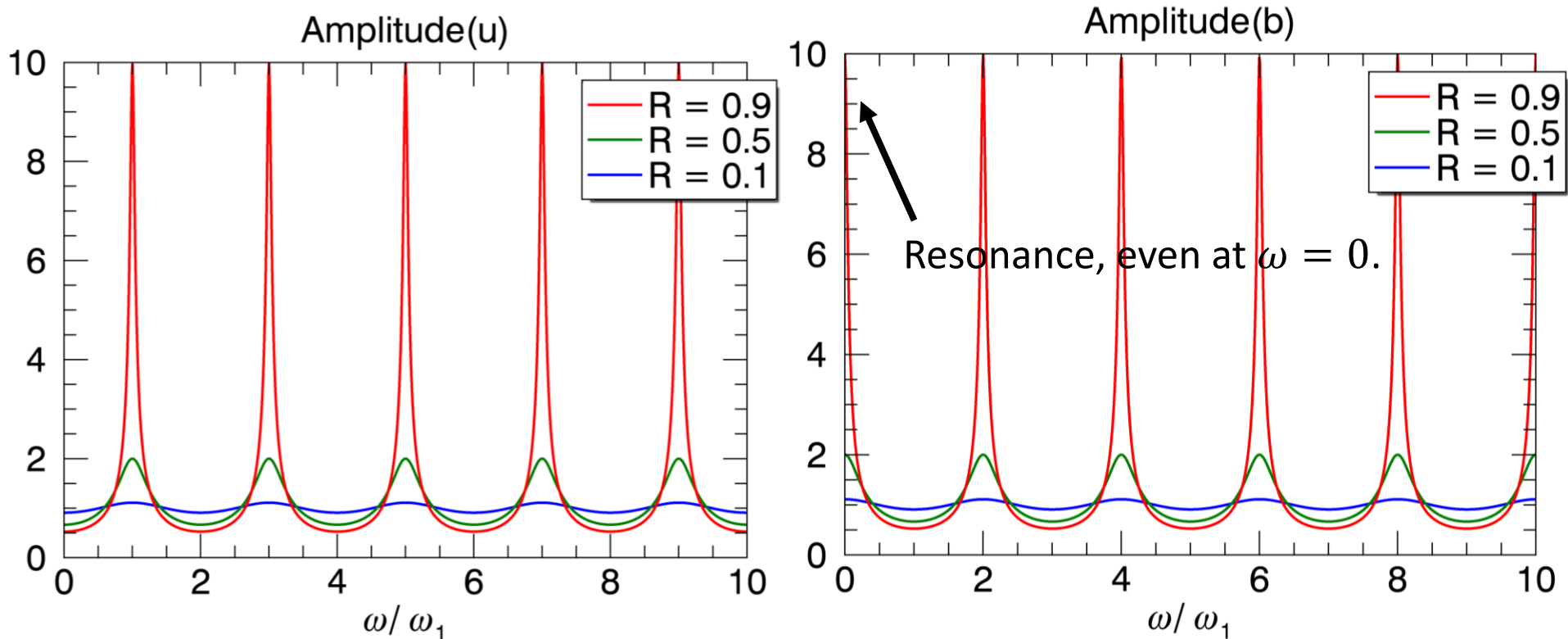
$= 0, t \rightarrow \infty$

$$u(0, t) = \frac{e^{i\omega t}}{1 + R e^{-2i\omega l/v_A}}$$

Geometric series
(converges for $R < 1$).

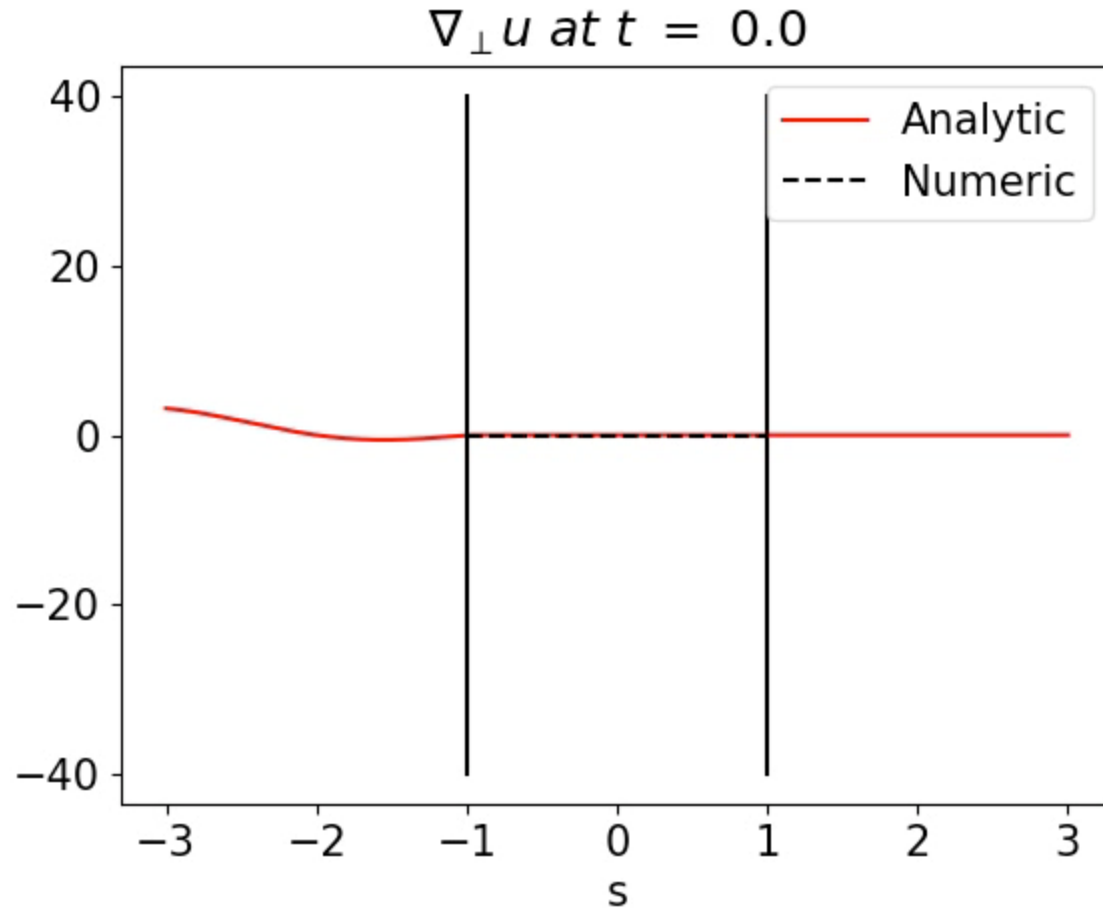
Steady-state amplitude at the loop apex

- Amplitude(u) = $\frac{1}{\sqrt{1+2R \cos\left(4\frac{\omega l}{v_A}\right)+R^2}}$,
- Amplitude(b) = $\frac{1}{\sqrt{1-2R \cos\left(4\frac{\omega l}{v_A}\right)+R^2}}$,
- Convergence timescale: $R^m = \exp\left(\left[\frac{t v_A}{L}\right] \ln R\right) \Rightarrow \tau \sim \frac{L}{v_A |\ln R|}$.



Does $\nabla_{\perp} u$ reach a steady-state?

- Yes (for $R < 1$).
- Same is true for $\nabla_{\parallel} u$.
- Amplitude of discontinuity initially grows linearly then decays exponentially.



Amplitude($\nabla_{\perp}u$) vs Amplitude($\nabla_{\parallel}u$)

- Key point: ∇u (and ∇b) tends towards a steady-state.
- Since the plasma is ideal, phase mixing is solely responsible for the build-up in ∇_{\perp} .
- If we can relate $\nabla_{\perp}u$ to $\nabla_{\parallel}u$ e.g.
$$\nabla_{\perp}u = C\nabla_{\parallel}u$$
- Then we know phase mixing has enhanced the gradients by a factor C .

Amplitude($\nabla_{\perp} u$) vs Amplitude($\nabla_{\parallel} u$)

At steady-state

$$\text{Amp}(\nabla_{\perp} u) = \frac{l}{v_A} \nabla_{\perp} v_A \left| \frac{1 - R \exp\left(-i \frac{\omega L}{v_A}\right)}{1 + R \exp\left(-i \frac{\omega L}{v_A}\right)} \right|^2 \text{Amp}(\nabla_{\parallel} u).$$

$$\frac{1 - R}{1 + R} \leq \left| \frac{1 - R \exp\left(-i \frac{\omega L}{v_A}\right)}{1 + R \exp\left(-i \frac{\omega L}{v_A}\right)} \right| \leq \frac{1 + R}{1 - R}$$

Driven at even harmonic.

Driven at odd harmonic.

Amplitude($\nabla_{\perp} u$) vs Amplitude($\nabla_{\parallel} u$)

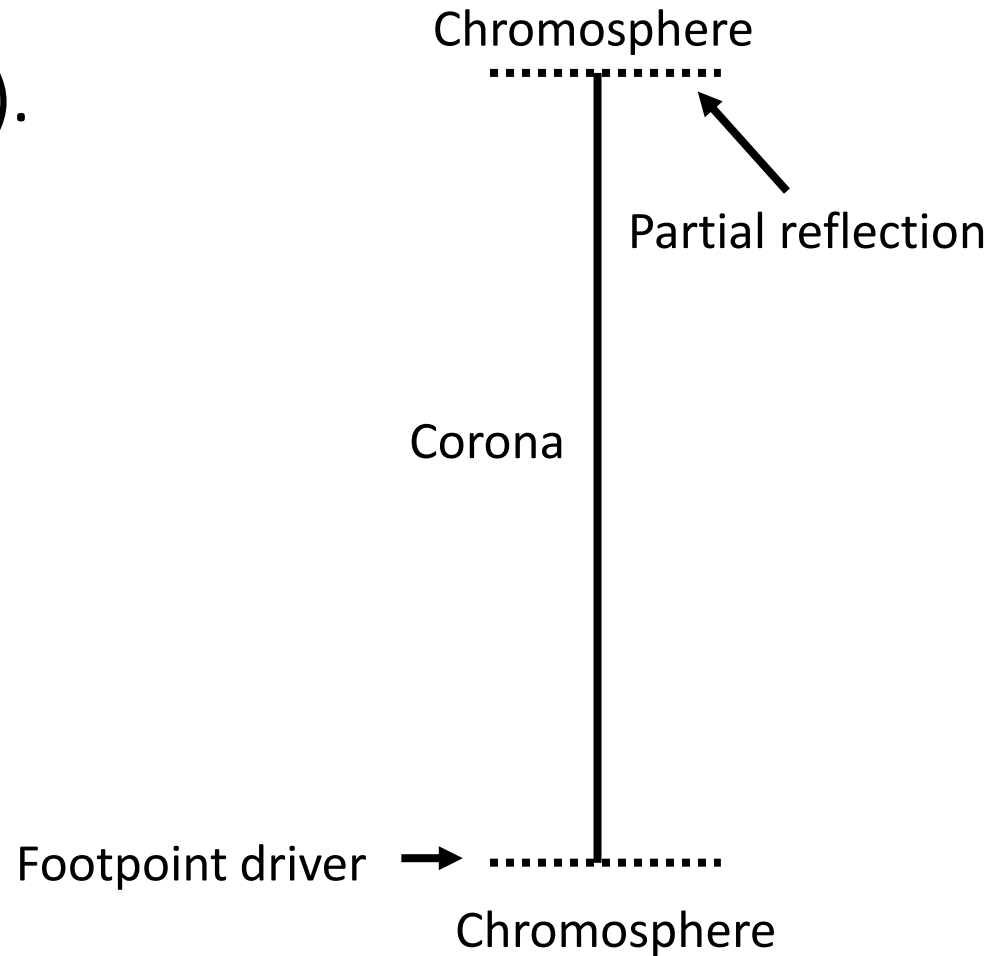
At steady-state

$$10^{-1} \text{Amp}(\nabla_{\parallel} u) \leq \text{Amp}(\nabla_{\perp} u) \leq 10^4 \text{Amp}(\nabla_{\parallel} u).$$

- If:
 - $l = 100 \text{ Mm}$,
 - $v_A = 400 \text{ km s}^{-1}$,
 - $\nabla_{\perp} v_A = 100 \text{ km s}^{-1} \text{ Mm}^{-1}$,
 - $R = 9/10$.
- Using a broadband driver could help reduce this range.

Experiment 3/3

- Parital reflection ($R < 1$).
- Broadband driver.



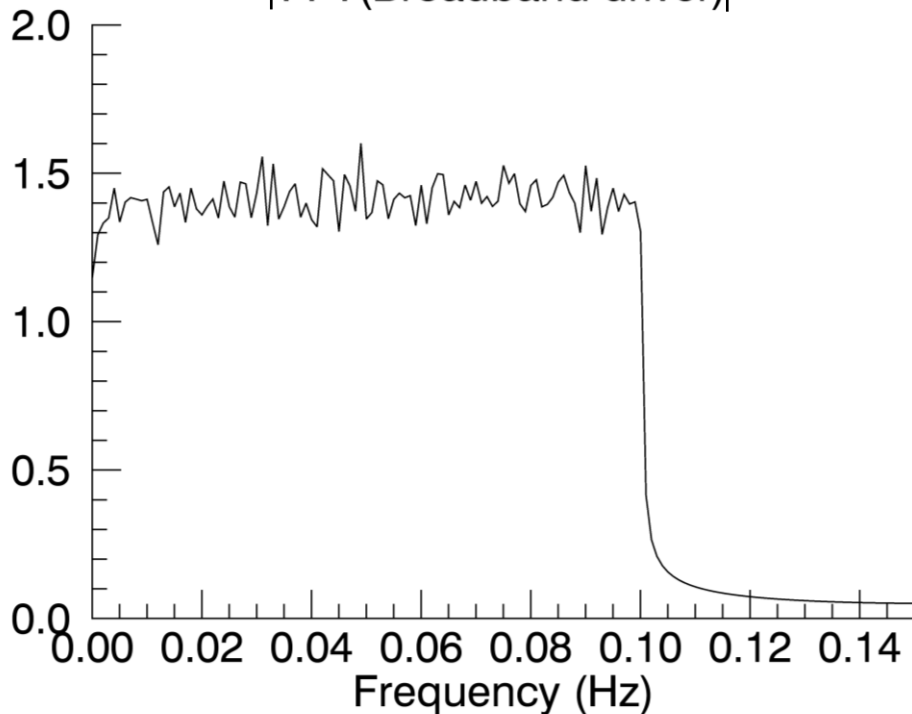
What is a broadband driver?

- A broadband driver is a driver which excites a range of frequencies.

$$u = \sum_{n=0}^N \sin(\omega_n t + \phi_n)$$

↑ Random phase.

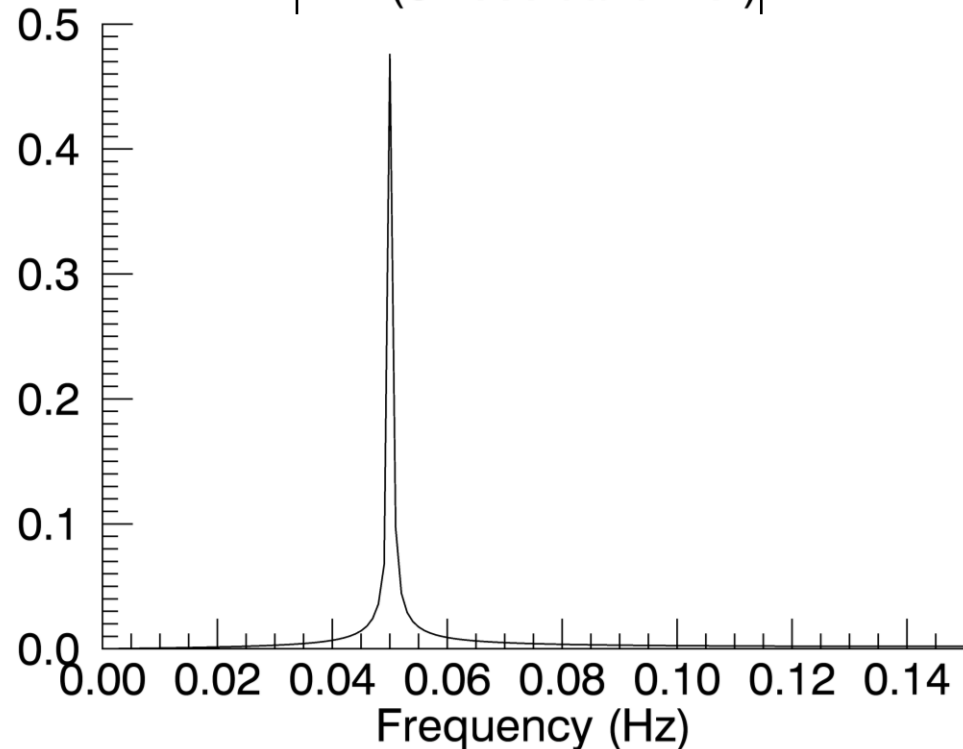
|FFT(Broadband driver)|



$$u = \sin(\omega t)$$

↑

|FFT(Sinusoidal driver)|



Analytic solution

- We have a solution for a sinusoidal driver, at steady state:

$$u(0, t) = \text{Amp}(\omega, R) \sin(\omega t) .$$

- Our driver now has the form:

$$u_{driv}(t) = \sum_{n=1}^N f_n^{-\alpha} \sin(\omega_n t + \phi_n) .$$

- So the solution is:

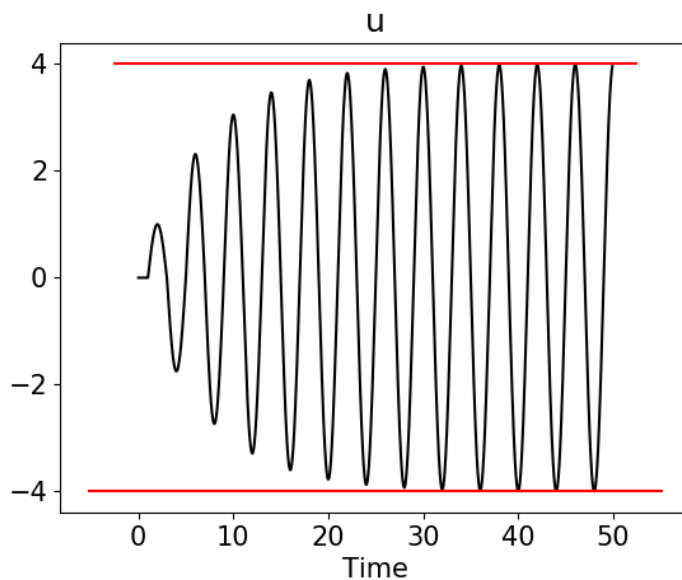
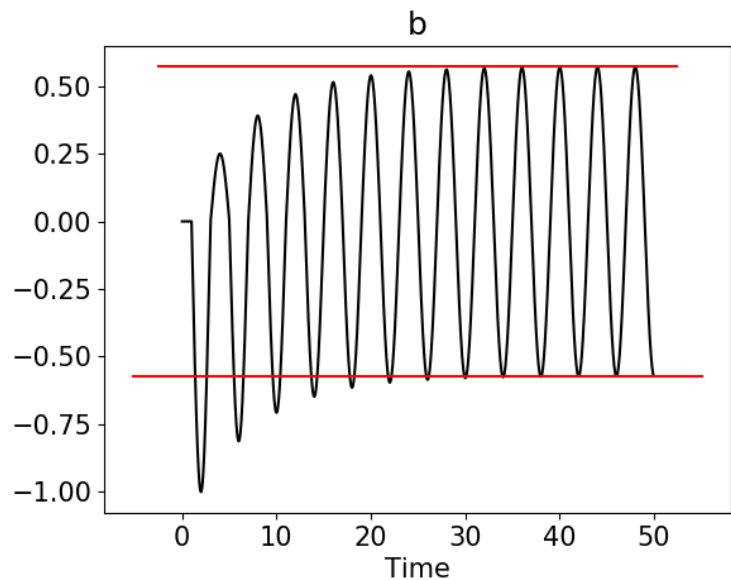
$$u(0, t) = \sum_{n=1}^N f_n^{-\alpha} \text{Amp}(\omega_n, R) \sin(\omega_n t + \phi_n) .$$

Gives $\sqrt{\text{power spectrum}}$.

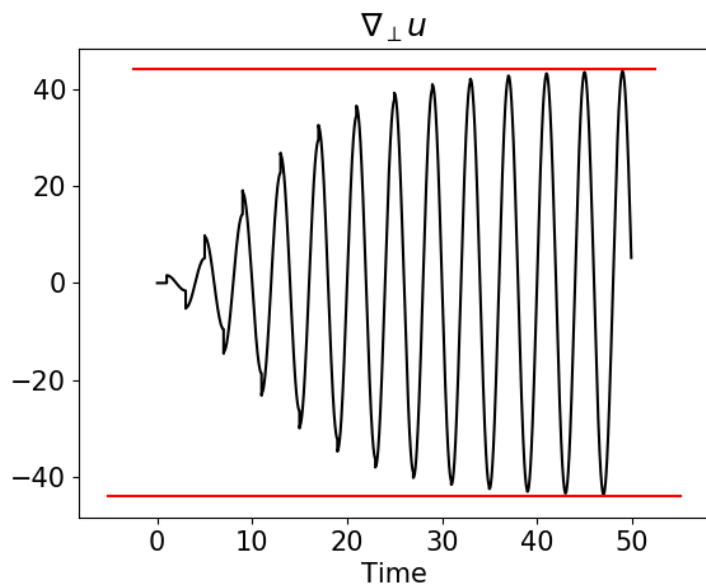
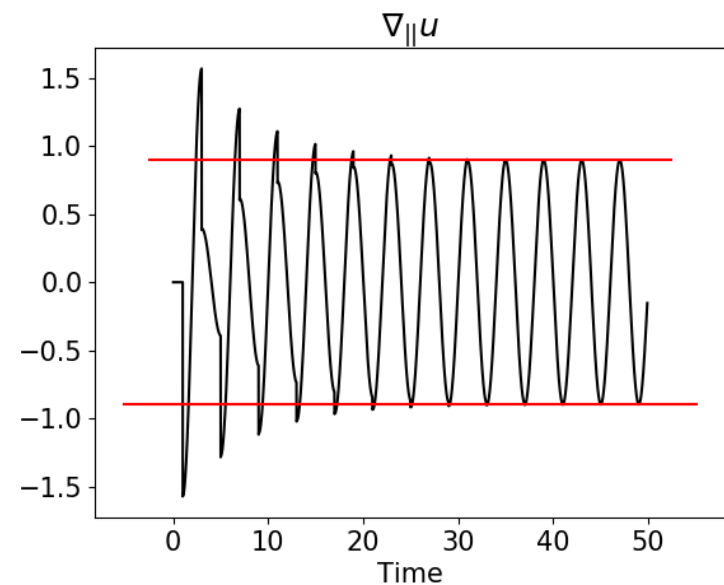
Why no numerical solution?

- Not yet had time.
- We have checked the analytic formula for sinusoidal drivers.
- Linear problem \implies solution is a superposition of the sinusoidal driver experiments.

Formula check



— Numerical solution
— Analytic
— predicted amplitude



The driver

- Takes the form,

$$u_{driv}(t) = \sum_{n=1}^N f_n^{-\alpha} \sin(\omega_n t + \phi_n).$$

Gives $\sqrt{\text{power spectrum}}$.

- $N = 1000$.

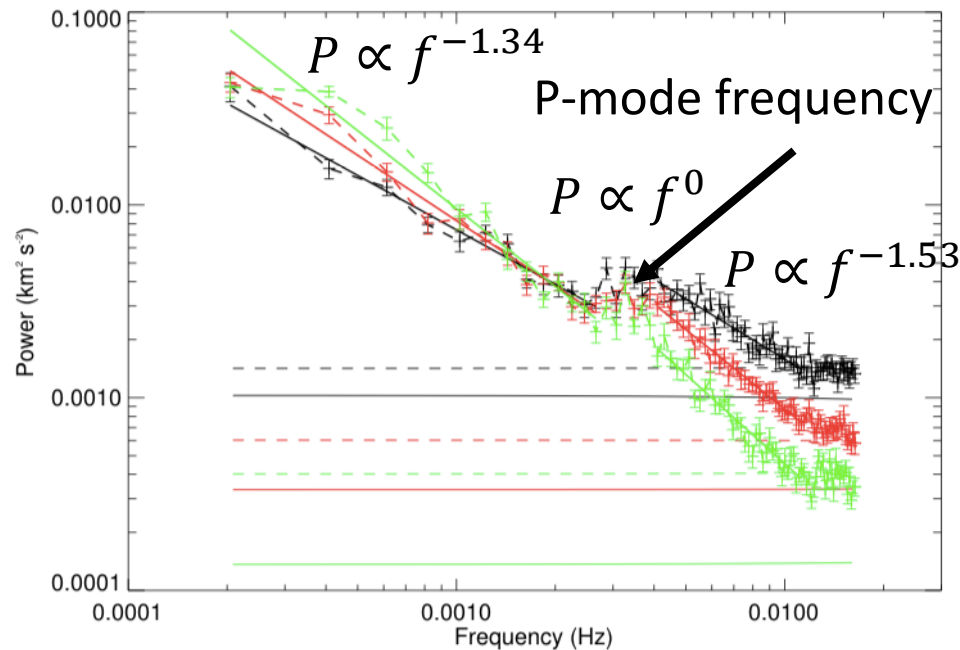
- $f_n = \frac{\omega_n}{2\pi} = n10^{-4}$ Hz

Can take any value.

- ϕ_n is a random phase with a uniform probability distribution over the interval $[0, 2\pi]$.

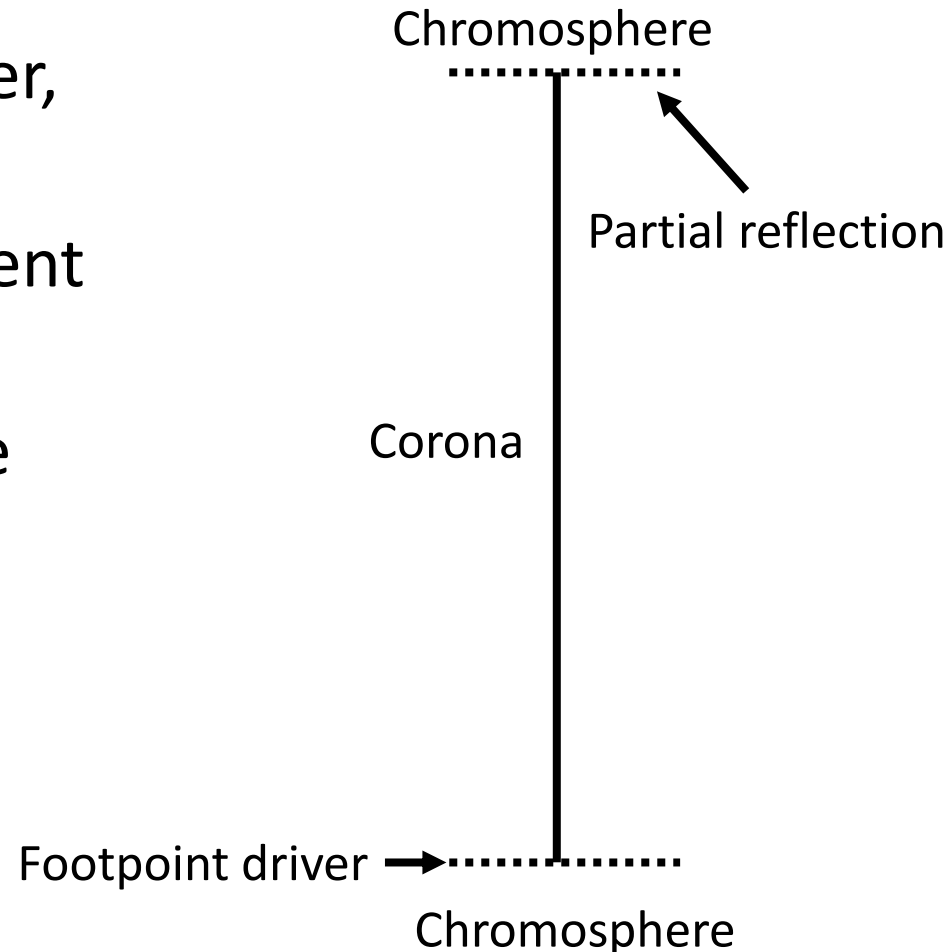
The driver

- Each term is multiplied by a factor $f_n^{-\alpha}$.
- $\alpha = [0.1, 0.5, 0.9]$ depending on the experiment.
- Since $u \propto \sqrt{P}$ we can see that $0 < \alpha < 1$.
- Results are mainly insensitive to our choice of α .



Experiment 3 - summary

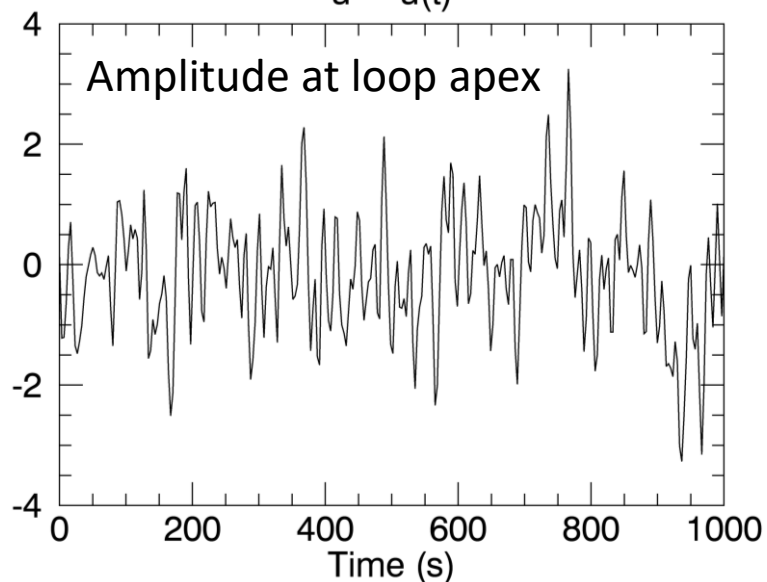
- Drive with a broadband driver, with a random phase.
- Repeat 1000 times and present the average.
- Use the analytic steady-state formulas.
- $L = 200\text{Mm}$.
- $v_A = 1\text{ Mm s}^{-1}$



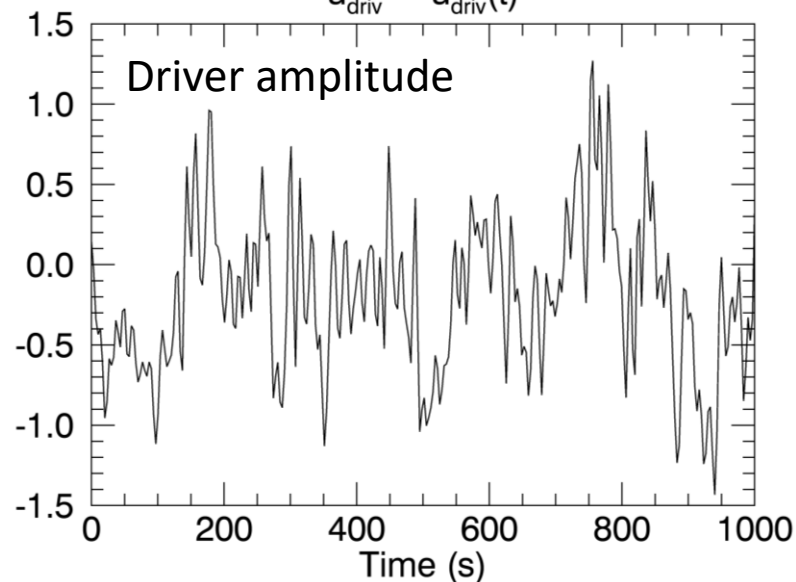
$R = 0.9, \alpha = 0.5$

Random experiment

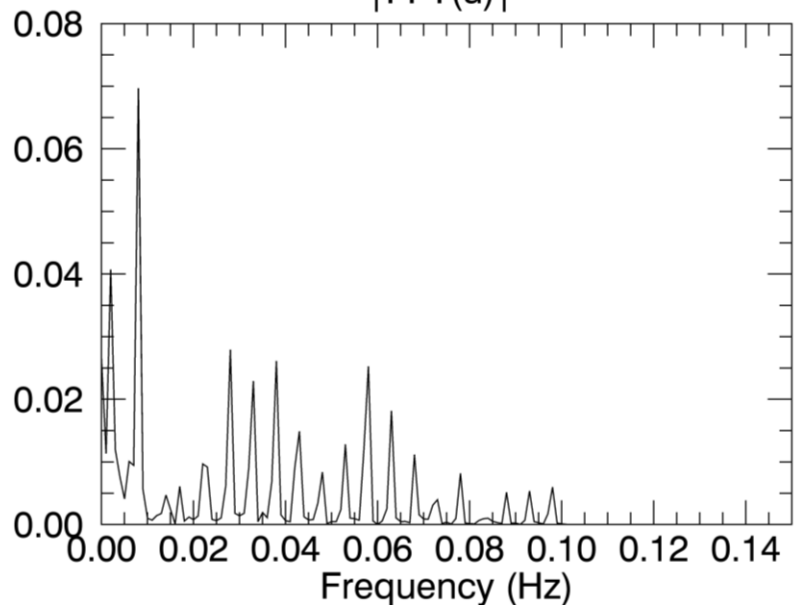
$u = u(t)$



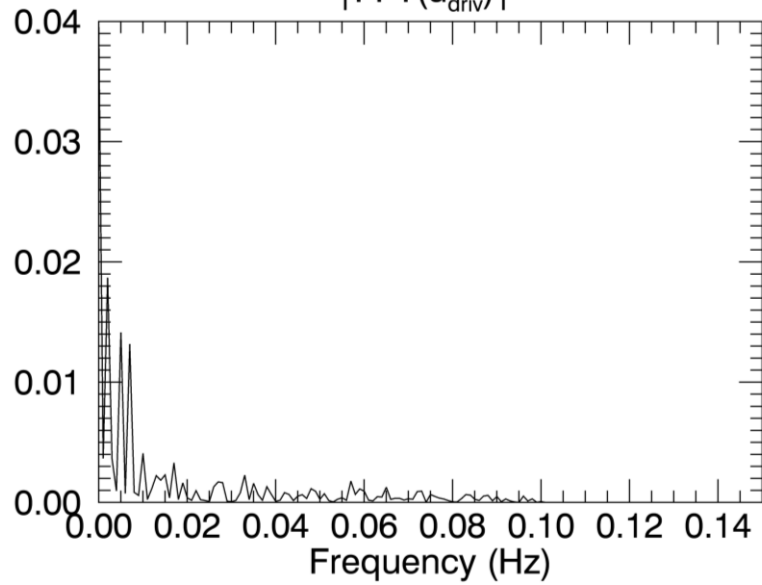
$u_{\text{driv}} = u_{\text{driv}}(t)$



$|\text{FFT}(u)|^2$

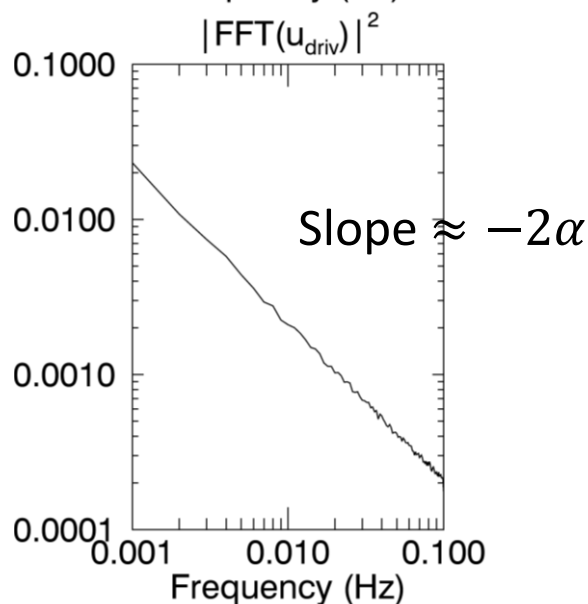
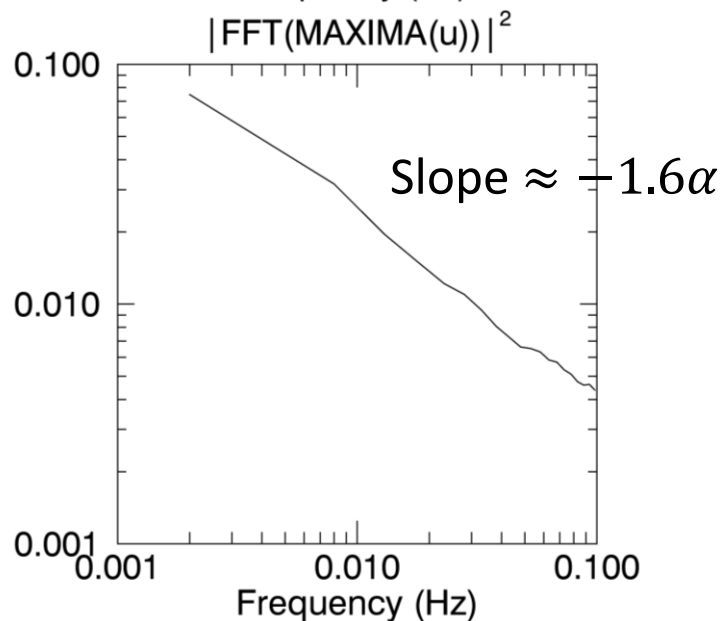
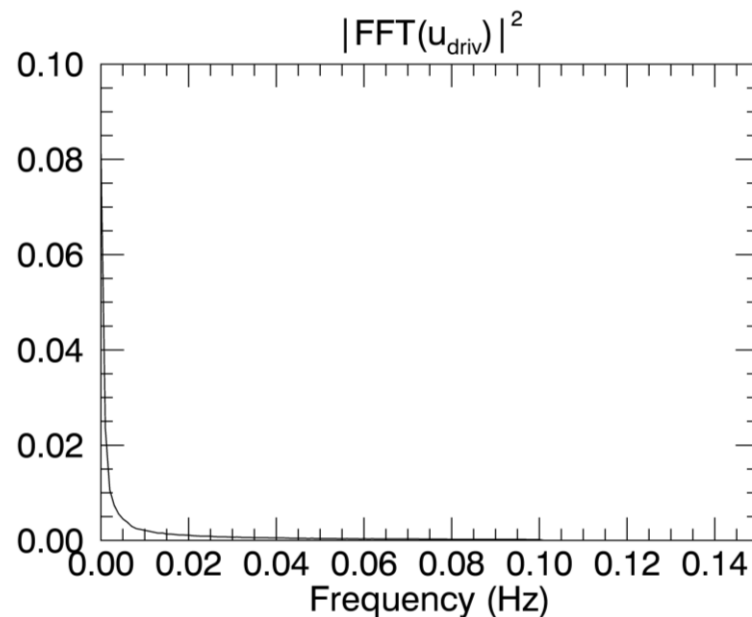
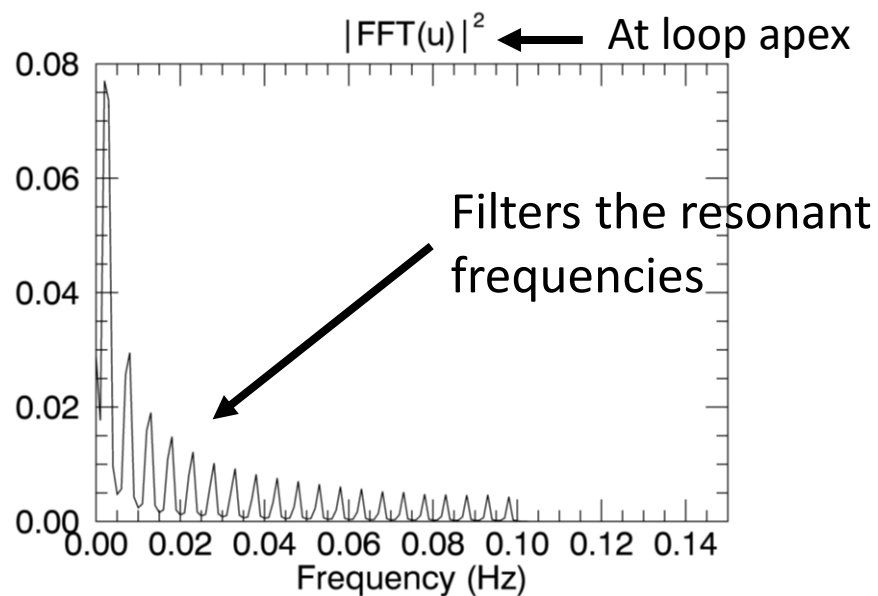


$|\text{FFT}(u_{\text{driv}})|^2$



$R = 0.9, \alpha = 0.5$

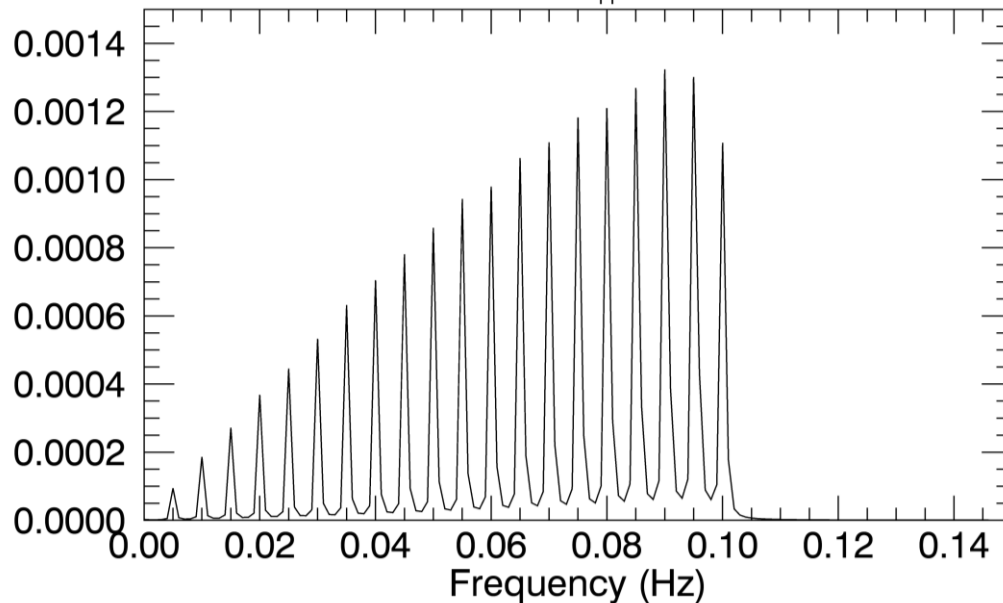
Average over 1000 experiments



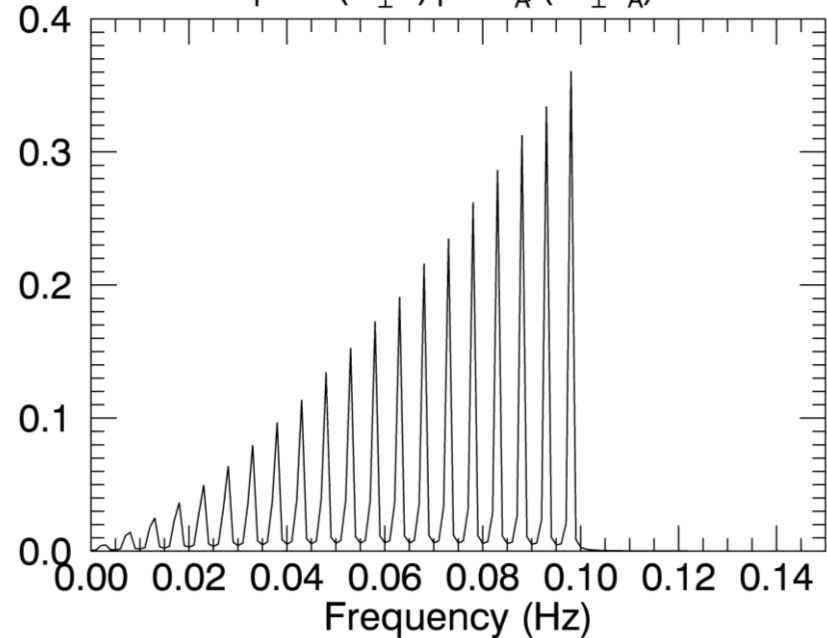
$$R = 0.9, \alpha = 0.5$$

Average over 1000 experiments

$$|\text{FFT}(\nabla_{\parallel} u)|^2$$



$$|\text{FFT}(\nabla_{\perp} u)|^2 \times v_A^2 / (|\nabla_{\perp} v_A|^2)$$



- Higher frequencies have the highest power.
- Sinusoidal driver:

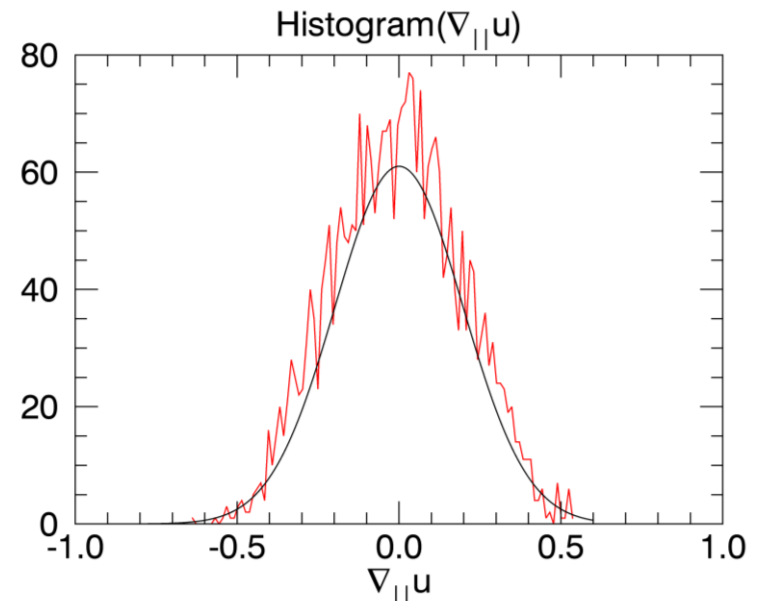
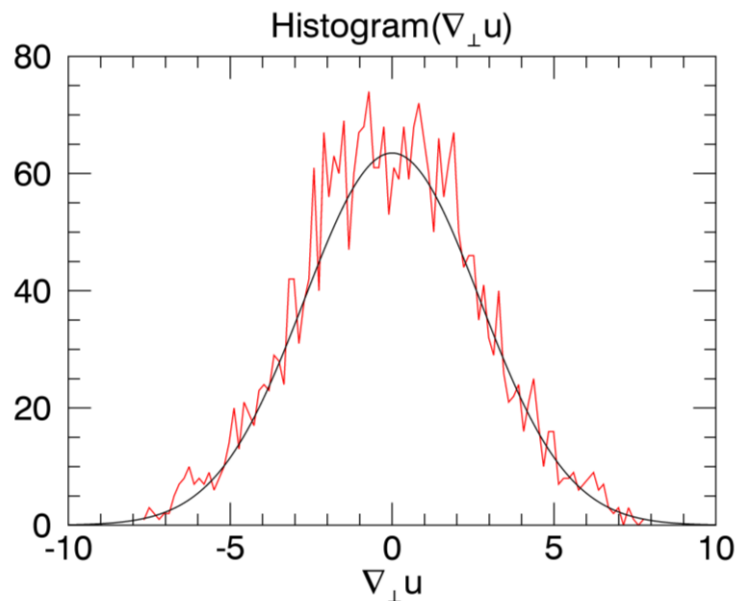
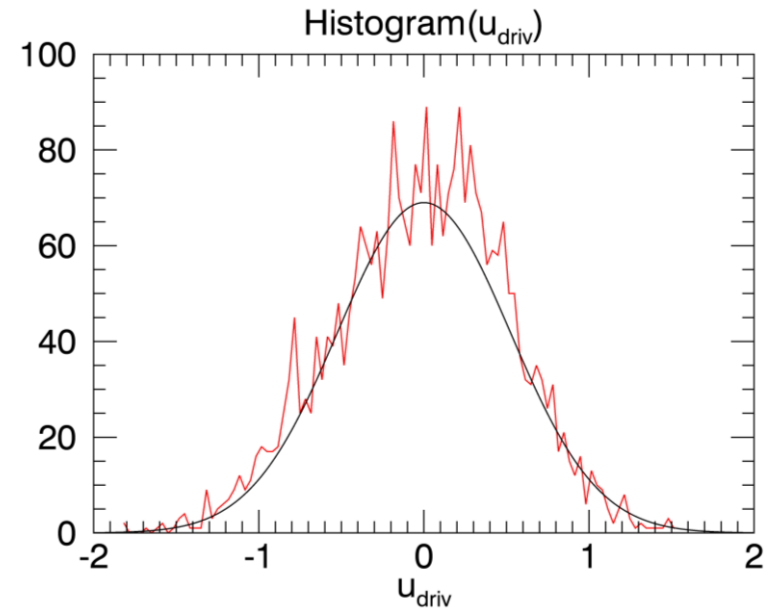
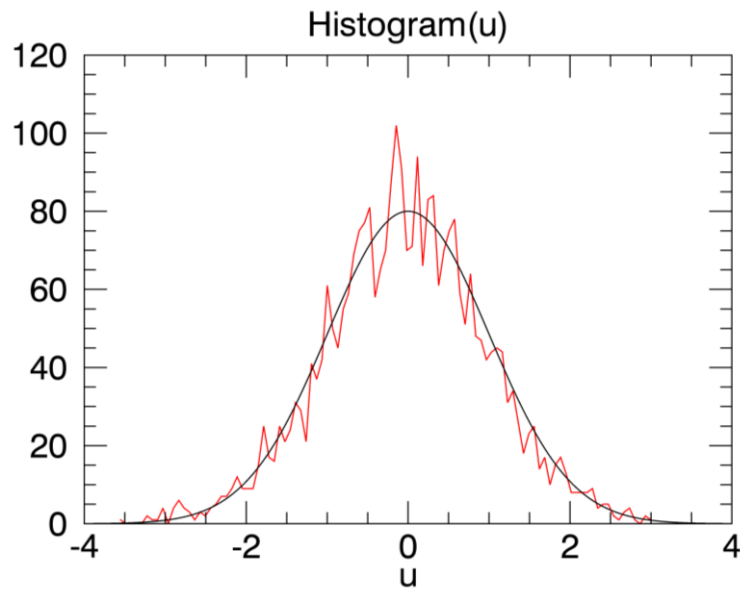
$$\nabla_{\parallel} u \propto \omega$$

- Broadband driver:

$$u_{driv,n} \propto \omega_n^{-\alpha}$$
$$\Rightarrow \nabla_{\parallel} u \propto \omega_n^{1-\alpha}$$

Values are \approx normally distributed

Random experiment, $R = 0.9, \alpha = 0.5$



Standard deviation of $\nabla_{||}u$ vs. $\nabla_{\perp}u$

- STD = standard deviation.
- Table of the average $\text{STD}(\nabla_{\perp}u)/\text{STD}(\nabla_{||}u)$:

	$\alpha = 0.1$	$\alpha = 0.5$	$\alpha = 0.9$	Analytic
$R = 0.5$	2.11	2.16	2.18	3
$R = 0.9$	14.0	13.7	13.8	19
$R = 0.99$	191	192	195	199
$R = 0.999$	1930	1950	1980	1999

- Proposed analytic formula (not proven):

$$\text{STD}(\nabla_{\perp}u) \approx \frac{l}{v_A} \nabla_{\perp} v_A \frac{1+R}{1-R} \text{STD}(\nabla_{||}u)$$

Simplifications

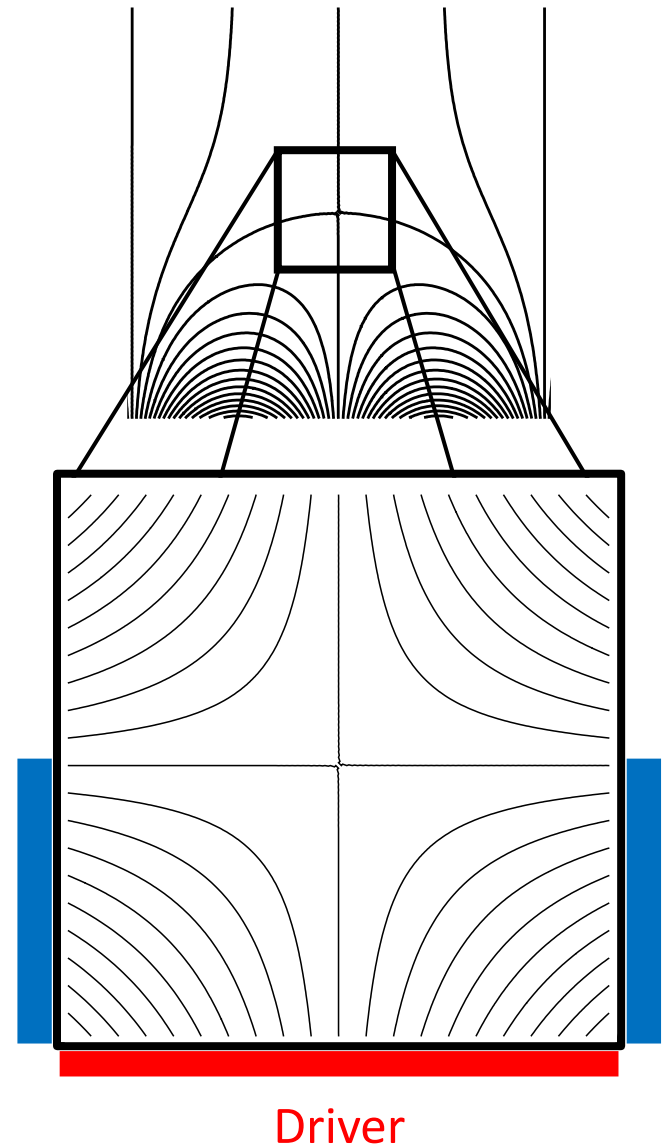
- We have a formula relating $\nabla_{\perp} u$ and $\nabla_{\parallel} u$.
- Assumed ideal MHD, therefore, our relation can be seen as an upper bound for $\nabla_{\perp} u$.
- However, these simplifications were also made:
 - Linear waves.
 - Consider only strict Alfvén waves.
 - $\nabla_{\parallel} v_A = 0^*$.
- Future work could look at the effects of modifying these simplifications.

Application of $\nabla_{\perp} u$ and $\nabla_{\parallel} u$ relation

X-point field

- Goal from previous work: Look at phase mixing due to variations in field line length.
- Formula could help deduce a parameter space where the phase mixing is negligible.

Partial reflection



Application of $\nabla_{\perp} u$ and $\nabla_{\parallel} u$ relation

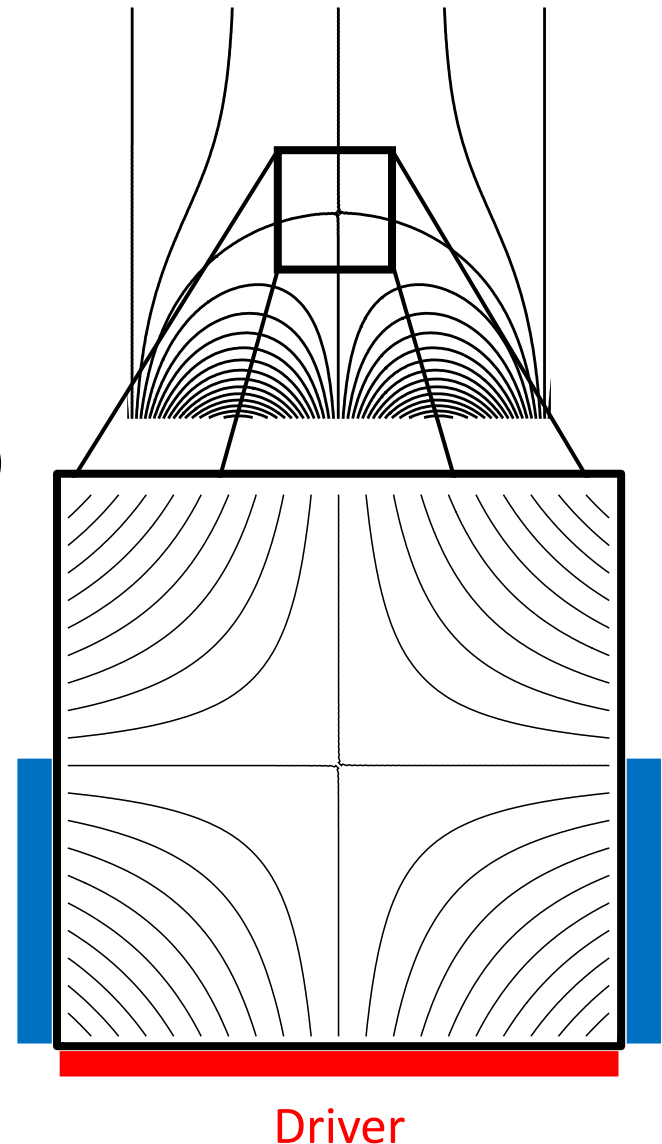
X-point field

- Calculated for a sinusoidal driver that:

$$\text{Amp}(\nabla_{\perp} u) = \left| \frac{1 - R \exp\left(-\frac{2i\omega l}{v_A}\right)}{1 + R \exp\left(-\frac{2i\omega l}{v_A}\right)} \right|^2 \text{Amp}(\nabla_{\parallel} u)$$

- Not confirmed numerically.
- Equation is not dependent on normalising constants.

Partial reflection



Summary

- We have derived a formula which links ∇_{\perp} and ∇_{\parallel} .
- In ideal MHD, phase mixing is only responsible for enhancing ∇_{\perp} .
- Therefore, it is hoped that our relation can be seen as an upper bound for the enhancement in heating due to phase mixing.

Future work

- Can we prove a formula for the relationship between $\text{STD}(\nabla_{\parallel} u)$ and $\text{STD}(\nabla_{\perp} u)$?
- Investigate the effects of switching to:
 - A nonlinear system.
 - 3D.
 - Other modes of oscillation.

Thank you for listening

Questions?